

Computational Models for the Growth of Closed Bacterial Cell Envelopes

Paul Schulze

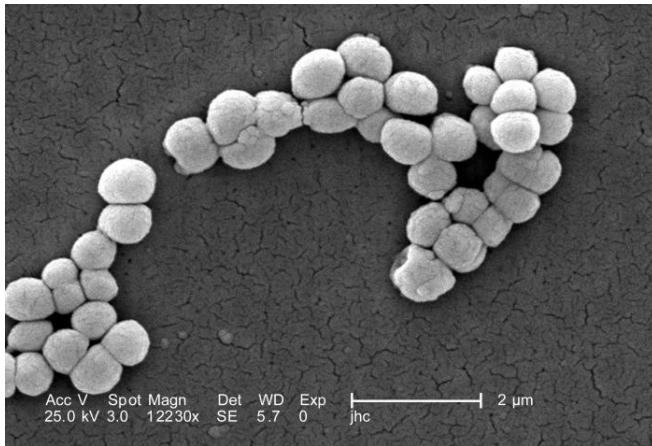
2023-01-19

Outline

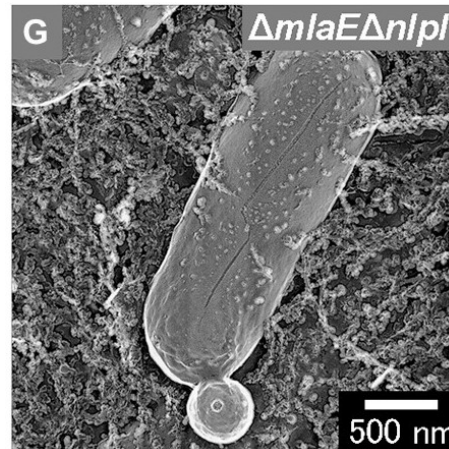
- Introduction
- Spring-based model
 - Idea behind the model
 - Results
- Finite-element-based model
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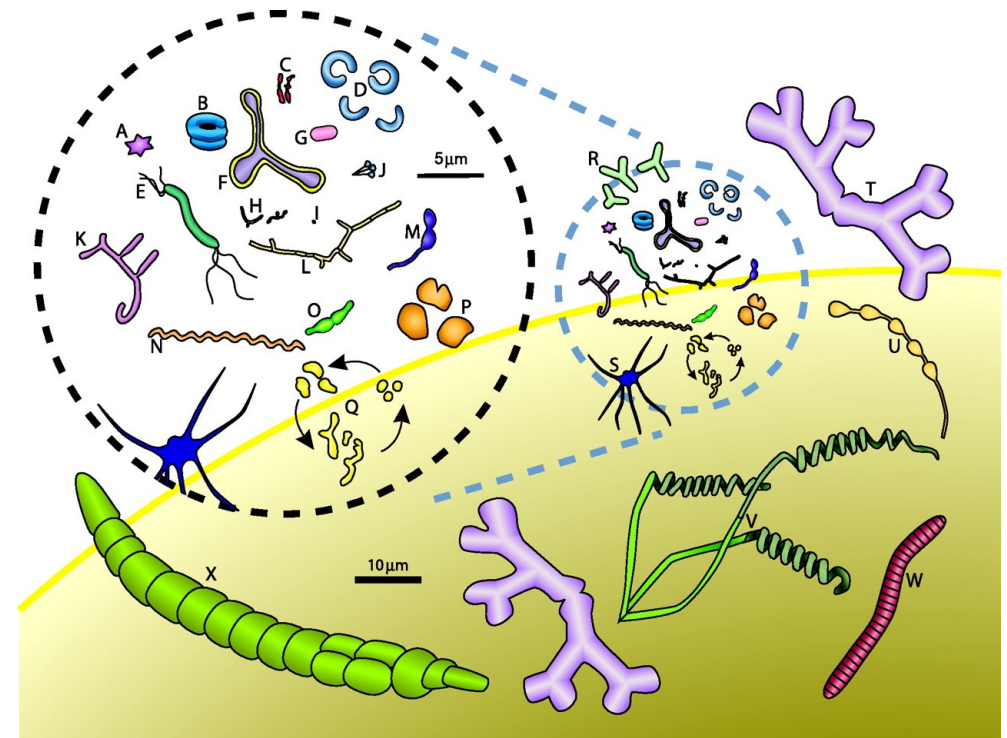
Shapes of bacteria



Carr, J. H. (2007) Public Health Image Library (PHIL), CDC



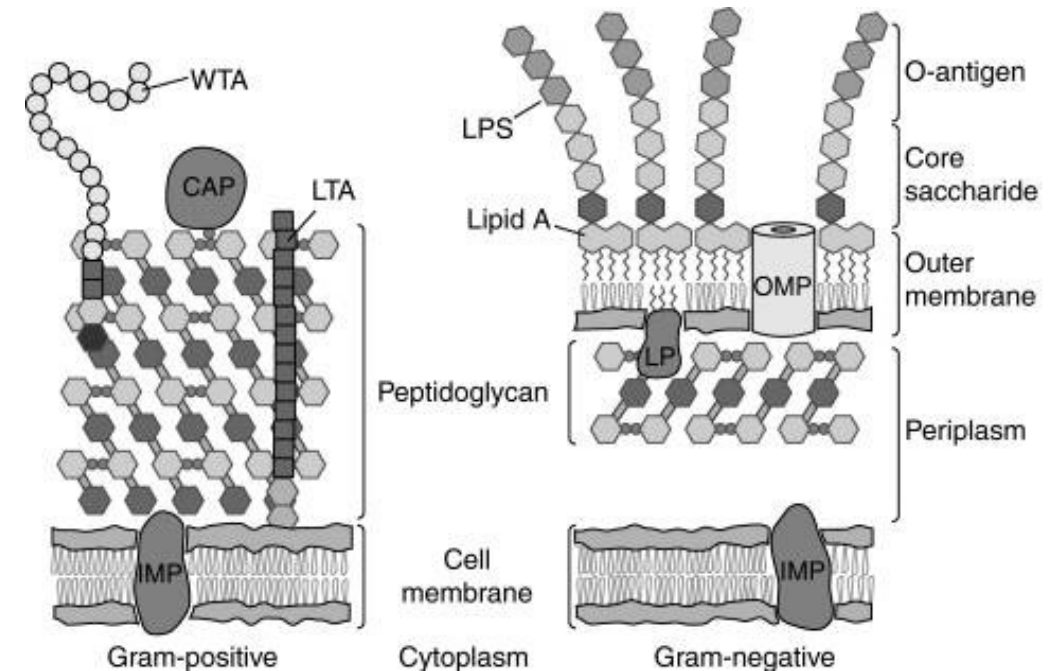
Ojima, Y. (2021) Microbial Physiology and Metabolism



Young, K. D. (2006) Microbiology and molecular biology reviews

The cell wall determines the shape

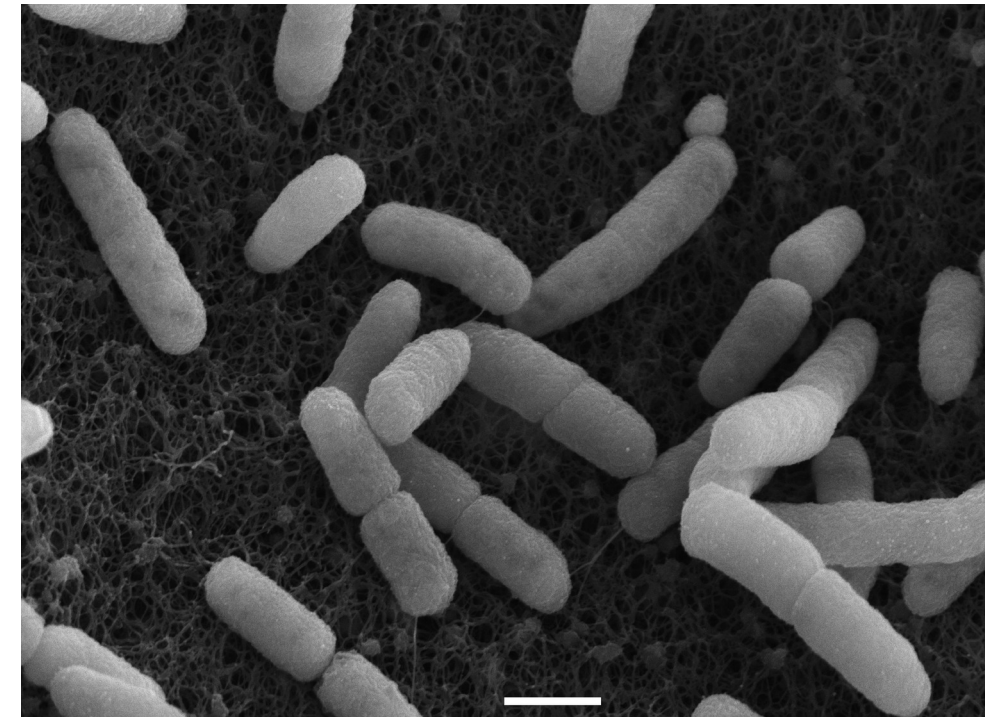
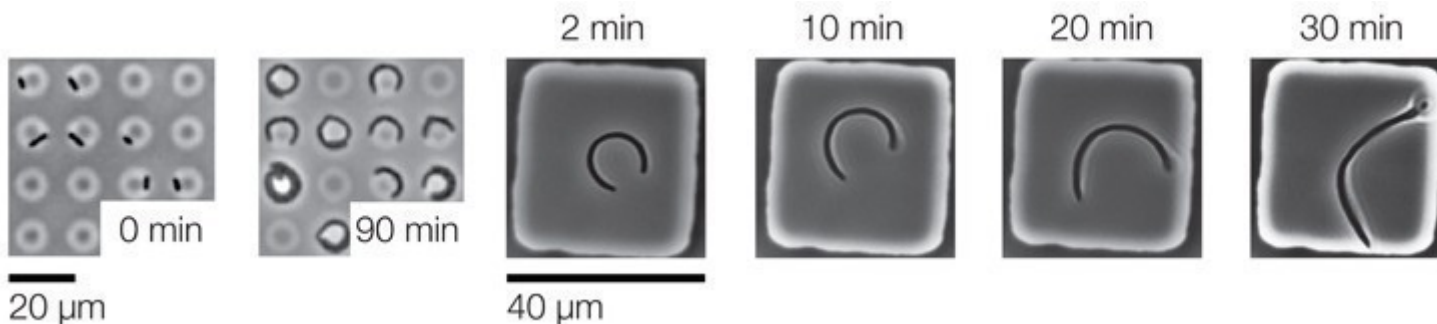
- Composed of Peptidoglycan
- Protects against *osmotic pressure*
- Two classes of bacteria
 - Gram-positive: Thick cell wall
 - Gram-negative: Thin cell wall



Silhavy, T.J. (2010) in Cold Spring Harbor perspectives in biology

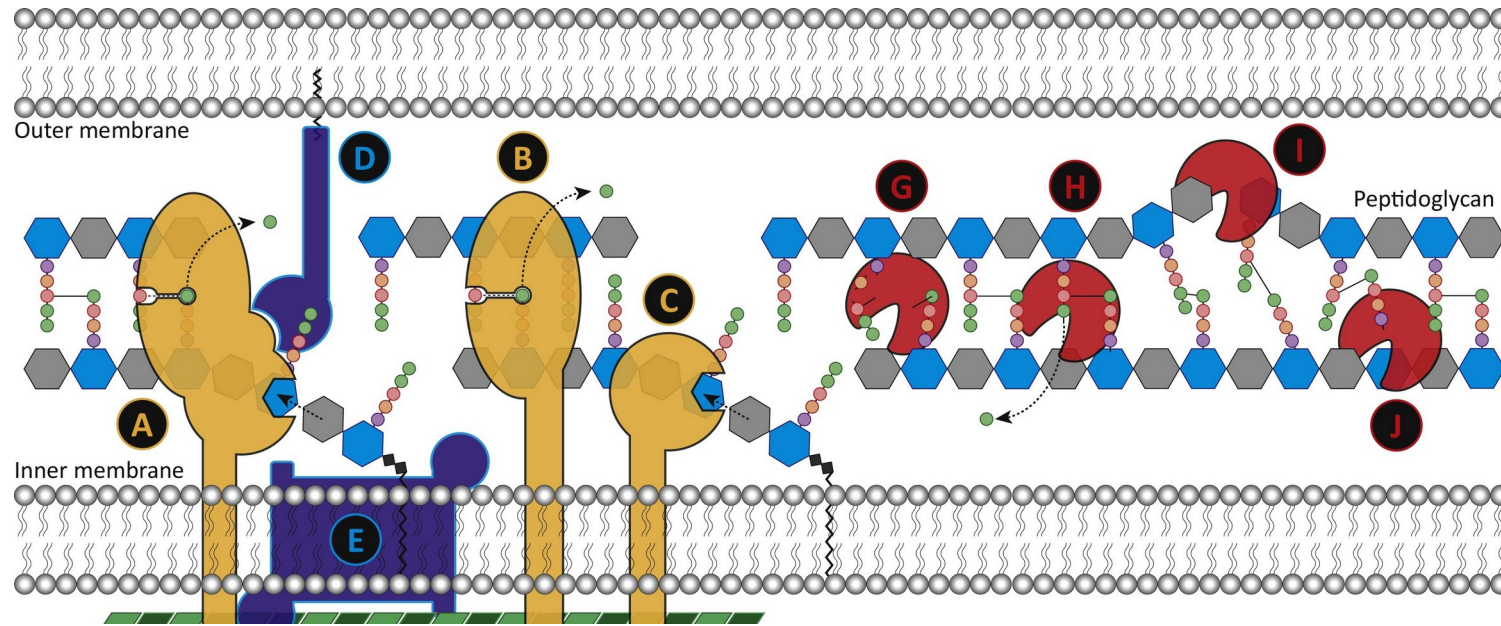
Shape preservation in bacteria

- Shape is consistent through generations
- Shape is recovered after disturbance
- Shape changes in response to the environment



Gudrun Holland, Michael Laue/RKI

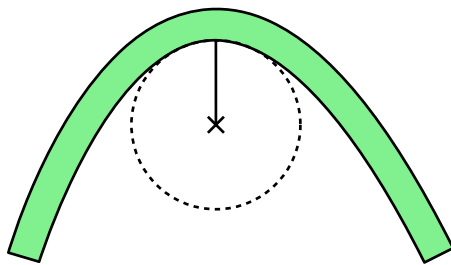
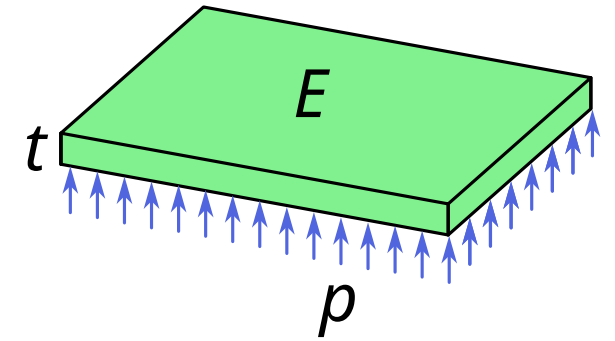
Peptidoglycan remodelling



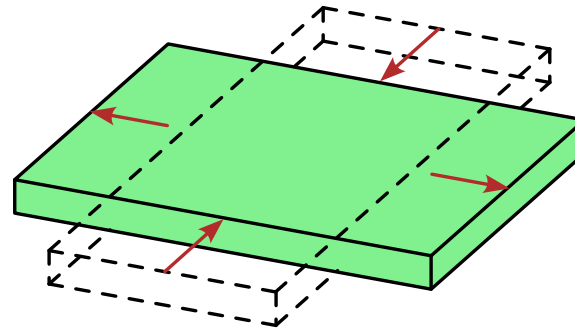
- **PG synthases** assemble the PG network
- **PG hydrolases** modify existing PG
- Guided by *mechanical / geometrical* cues?

Growth model for the bacterial shell

- Mechanical properties of the cell wall
- Turgor pressure
- Growth rates are based on local cues



Curvature



Strain

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Spring-based model of the shell

- Linear elastic continuum
 - Young's modulus E
 - Thickness t
- Spring network
 - Spring stiffness k_s
 - Bending stiffness k_b
- Mapping:

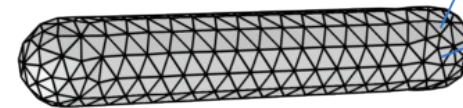
$$E, t \rightarrow k_s, k_b$$



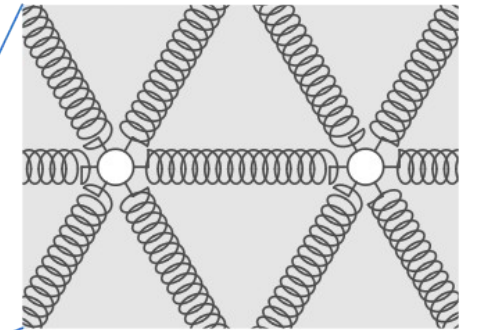
Cell shape



Linear elastic continuum

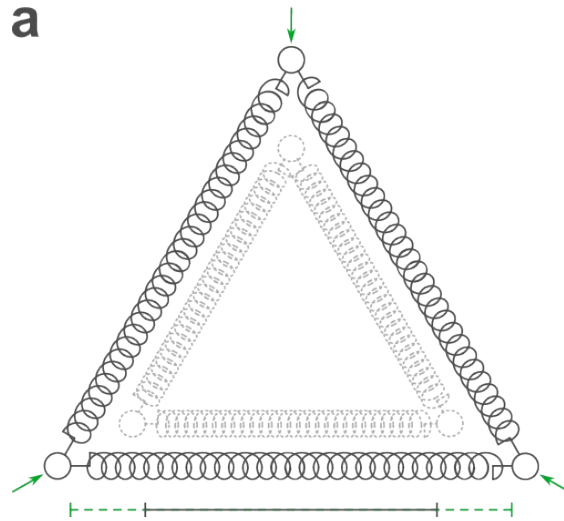


Triangulated surface

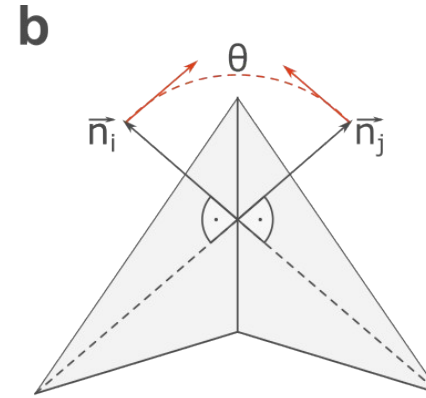


Linear elastic surface modelled as a network of Hookean springs.

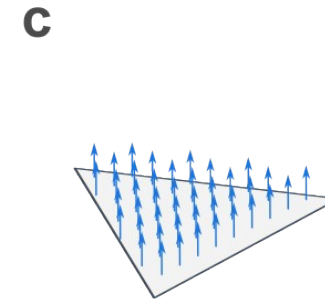
Energy function



Spring Energy



Bending Energy

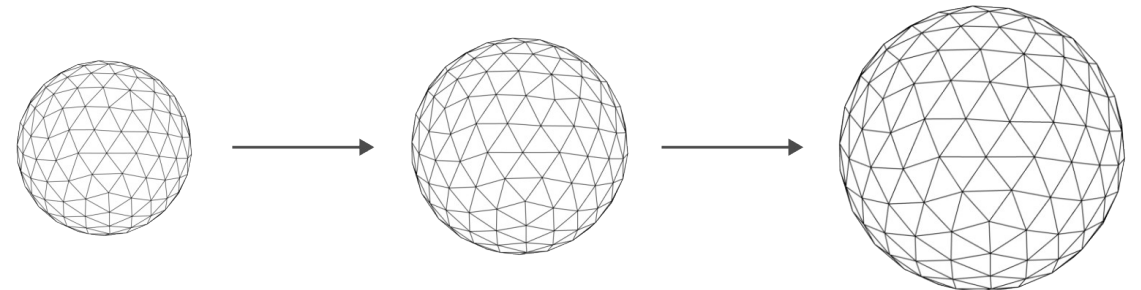
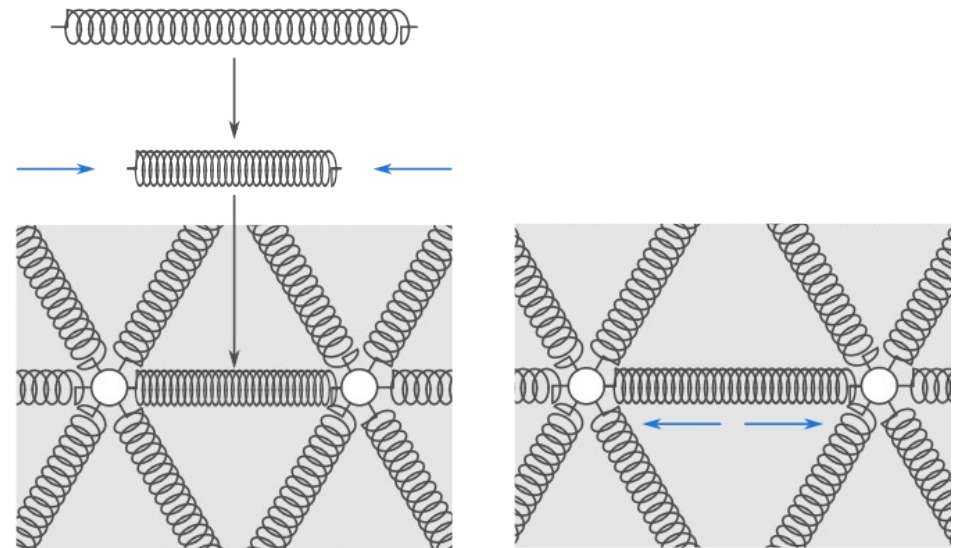


Pressure Energy

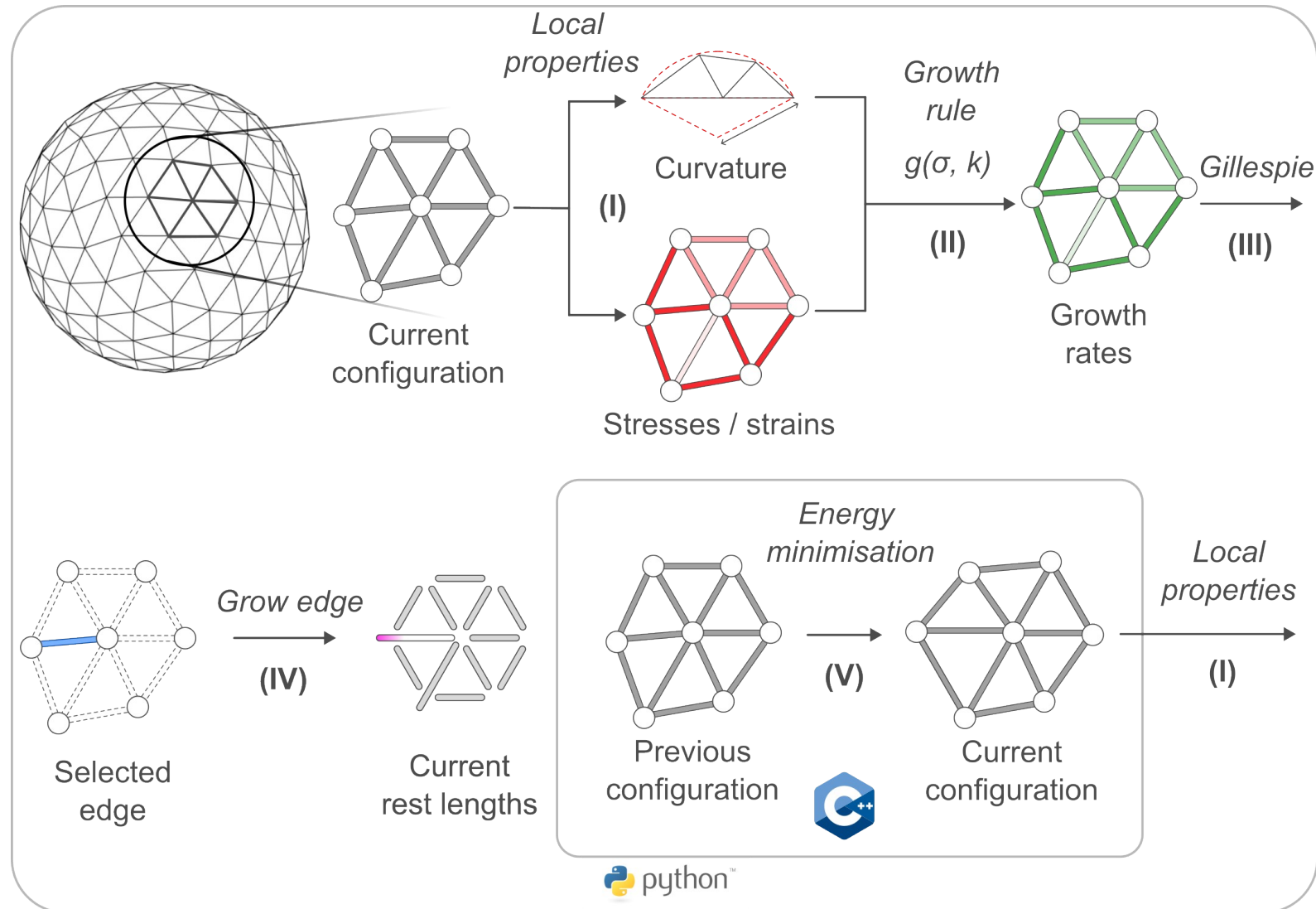
$$E = \sum_e^{\text{edges}} \frac{k_s}{2} (l_e - l_{0,e})^2 + \sum_{\{i,j\}(\text{adj.})}^{\text{triangles}} k_b (1 - \vec{n}_i \cdot \vec{n}_j) - pV$$

Iterative growth

- Increasing rest lengths $l_{e,0}$
- Mesh topology is consistent between growth steps

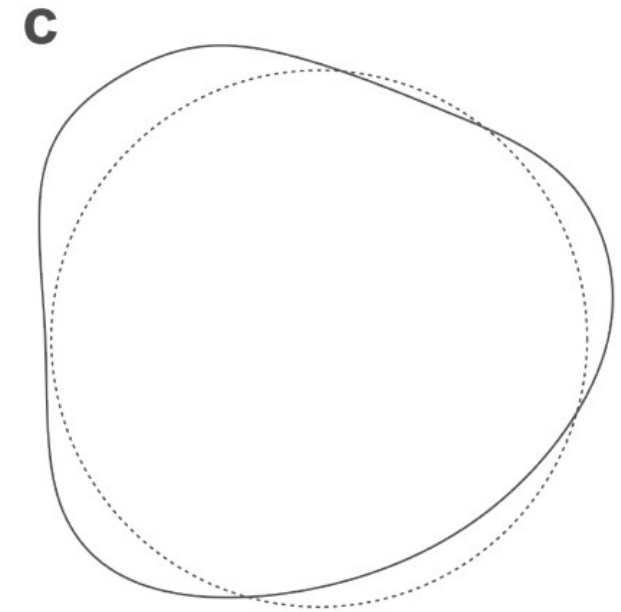
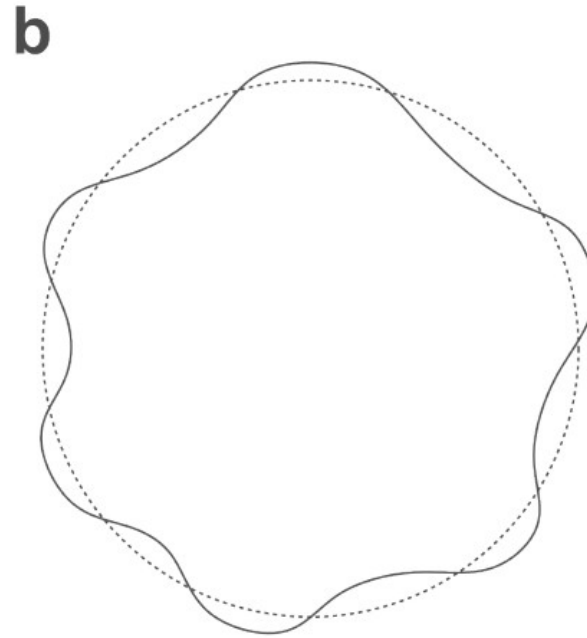
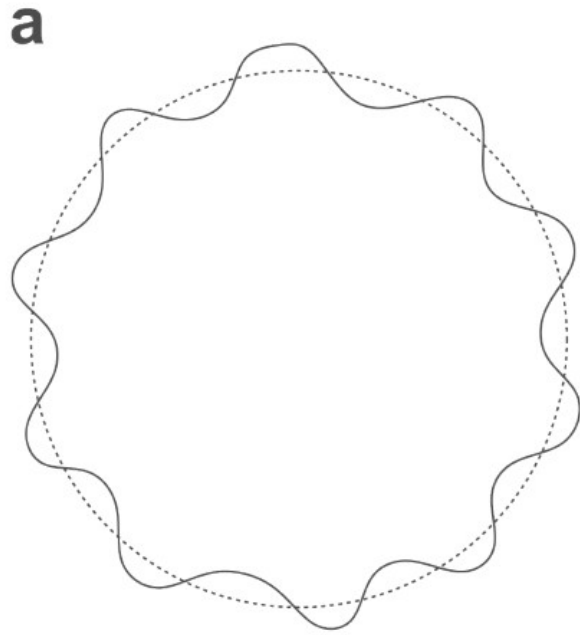


Simulation flowchart



- Introduction
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Observables



Roughness



Asphericity

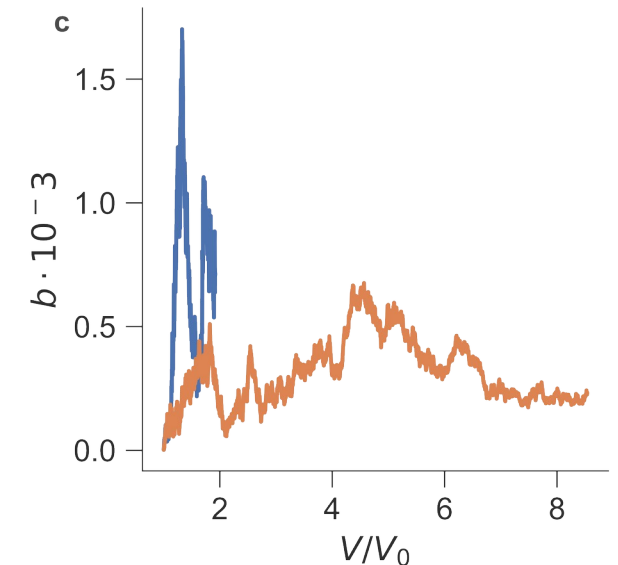
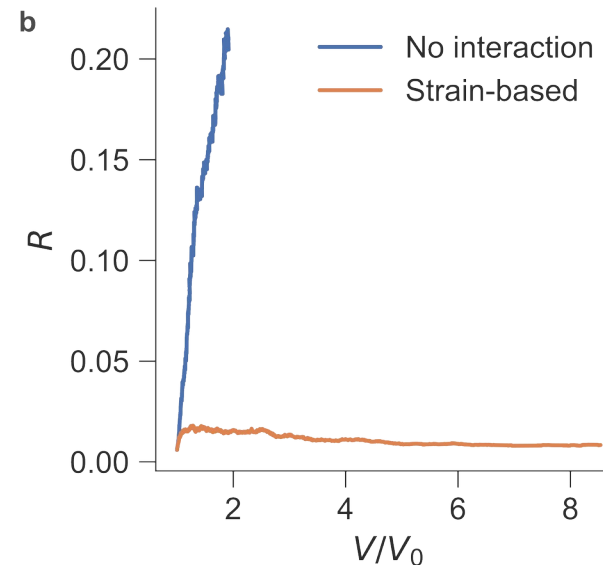
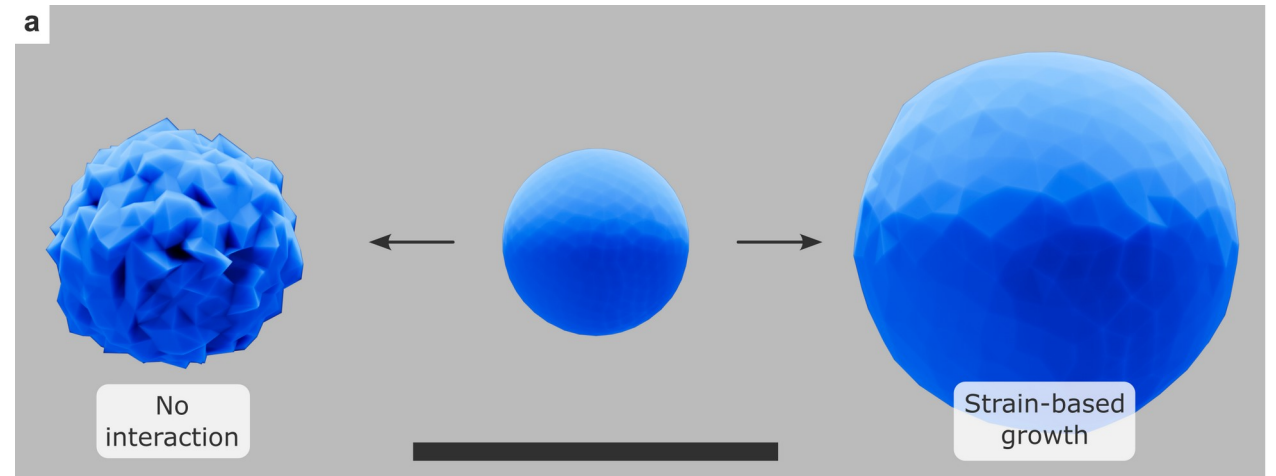


Random vs. strain-based growth

Strain-based growth rates:

$$\varepsilon_e = (l_e - l_{e,0})/l_{e,0}$$

$$\lambda_e = -\lambda_0 + \lambda_1 \varepsilon_e$$



Random vs. strain-based growth

Strain-based growth rates:

$$\varepsilon_e = (l_e - l_{e,0})/l_{e,0}$$

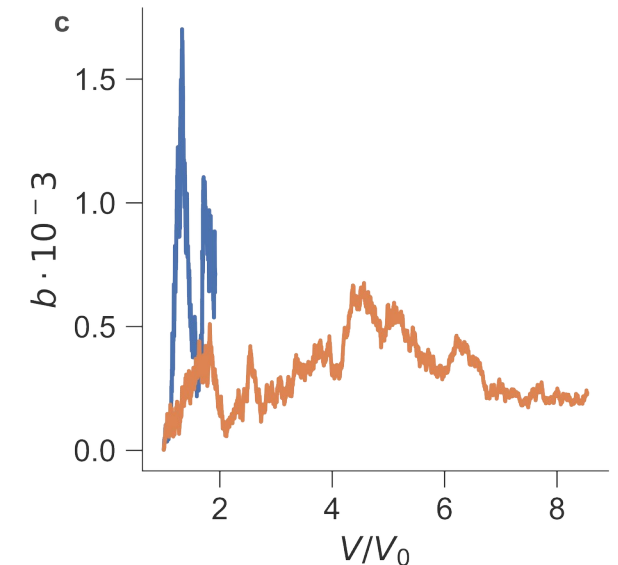
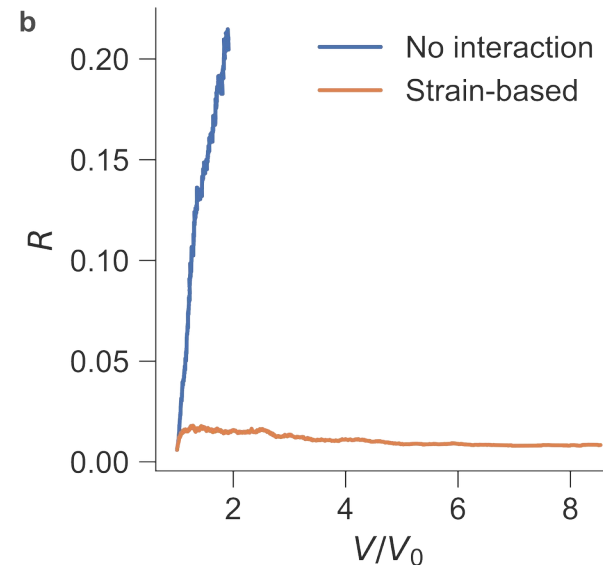
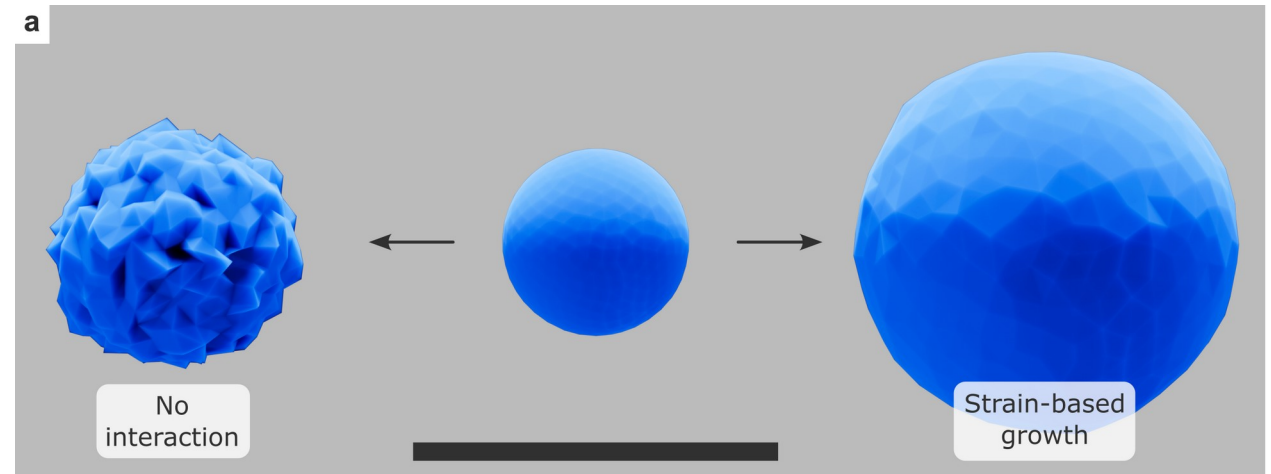
$$\lambda_e = -\lambda_0 + \lambda_1 \varepsilon_e$$

Random

- Spherical shape
- Surface **roughness**

Strain-based

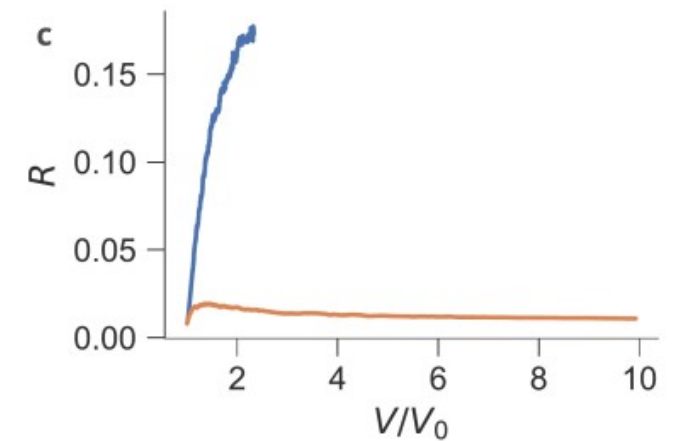
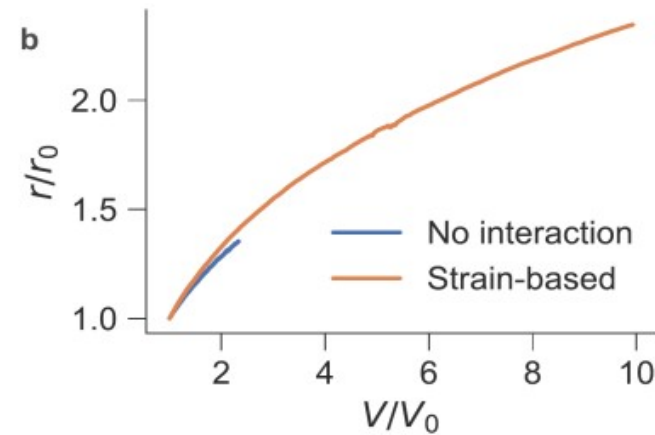
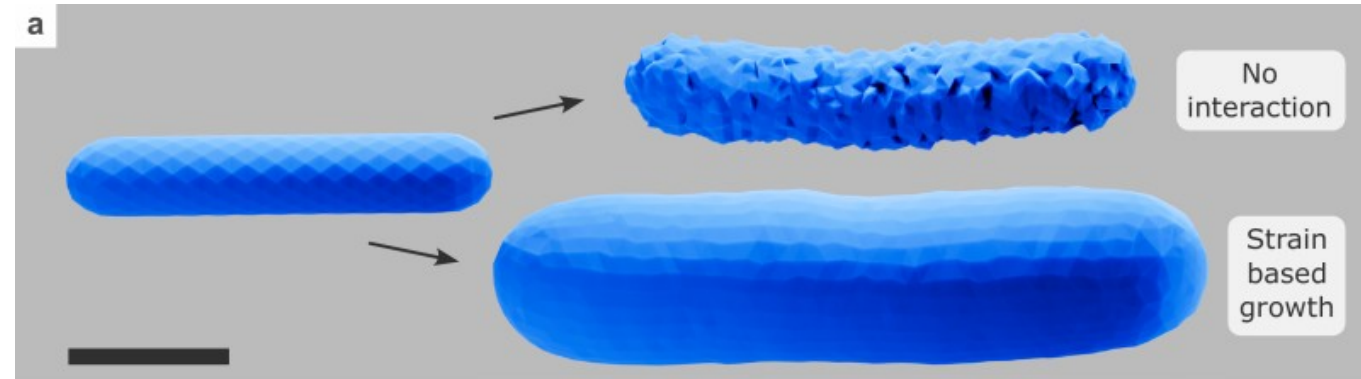
- Spherical shape
- **Smooth** surface



Random vs. strain-based growth

Strain-based growth rates:

$$\lambda_e = -\lambda_0 + \lambda_1 \varepsilon_e$$



Random vs. strain-based growth

Strain-based growth rates:

$$\lambda_e = -\lambda_0 + \lambda_1 \varepsilon_e$$

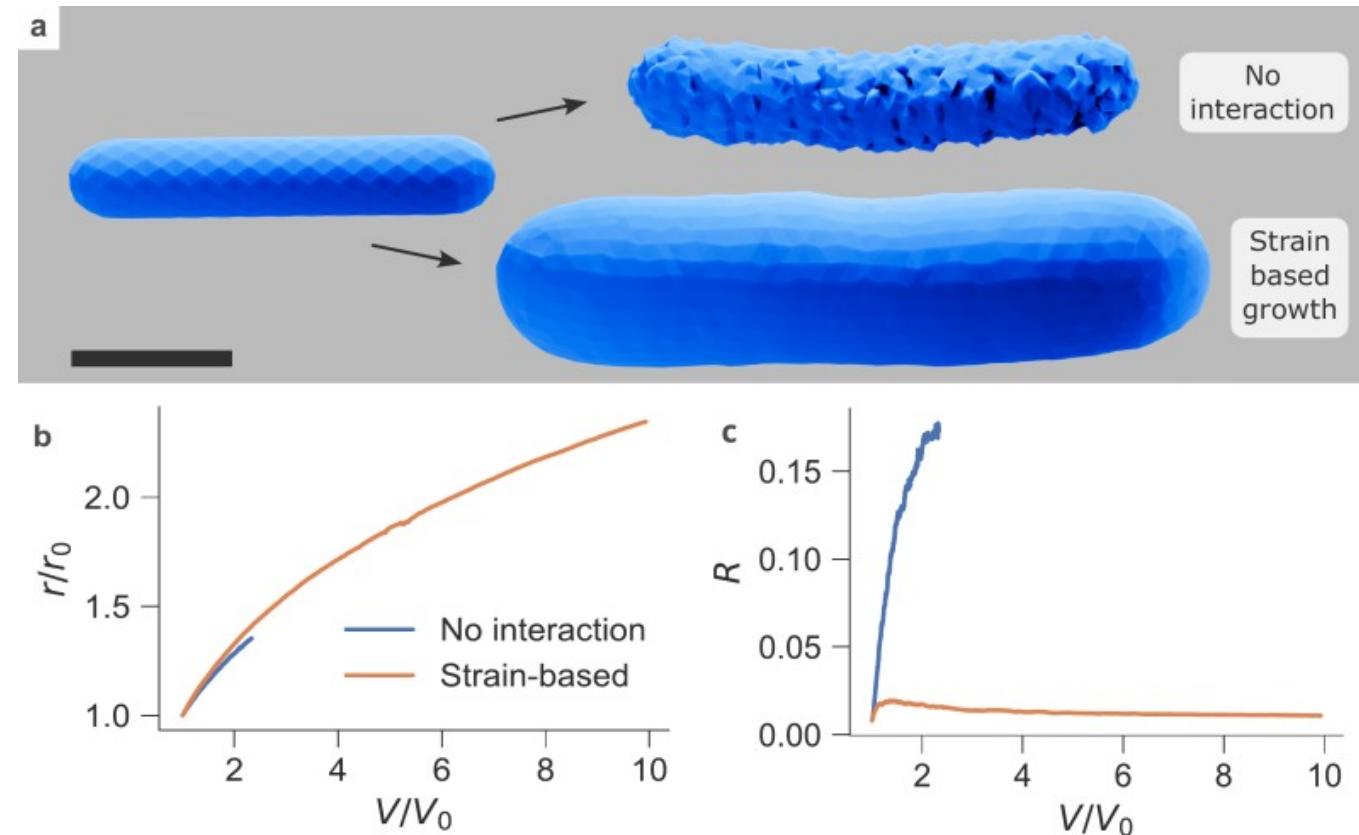
Random growth

- Cylindrical shape
- Surface **roughness**

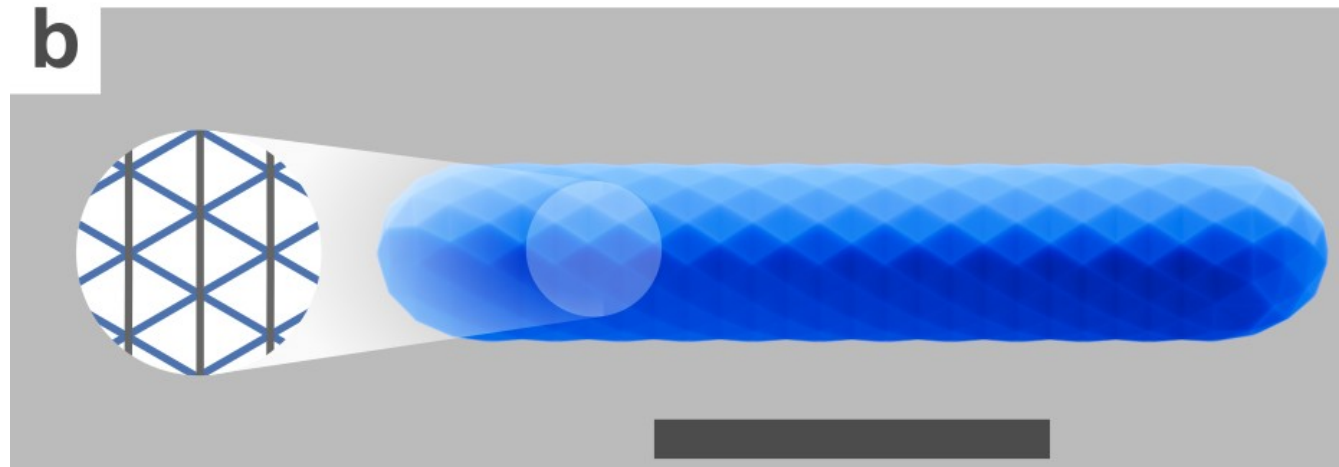
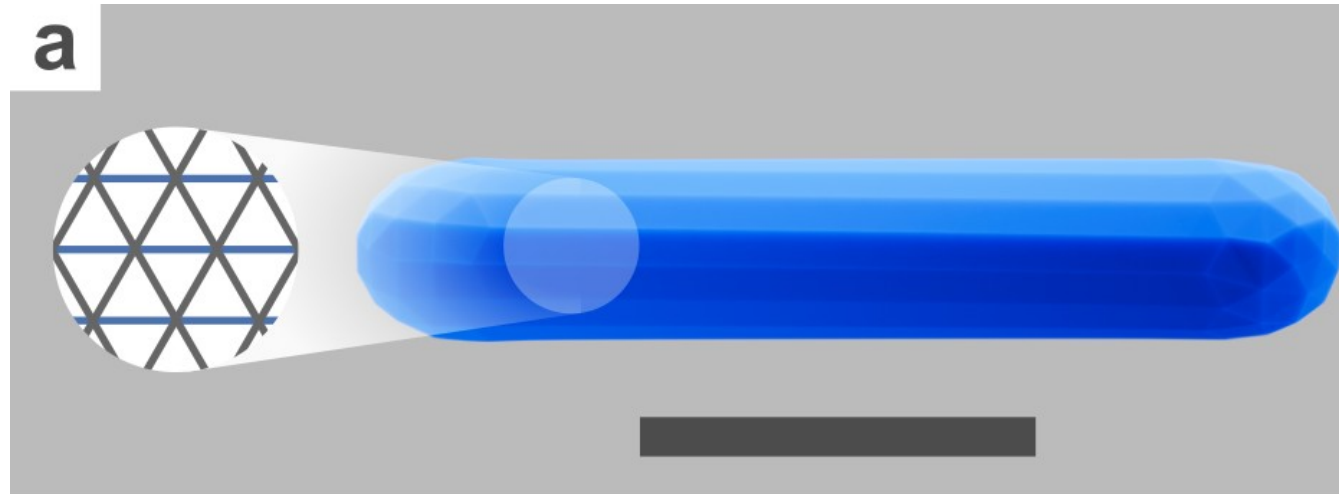
Strain-based growth

- Cylindrical shape
- **Smooth** surface

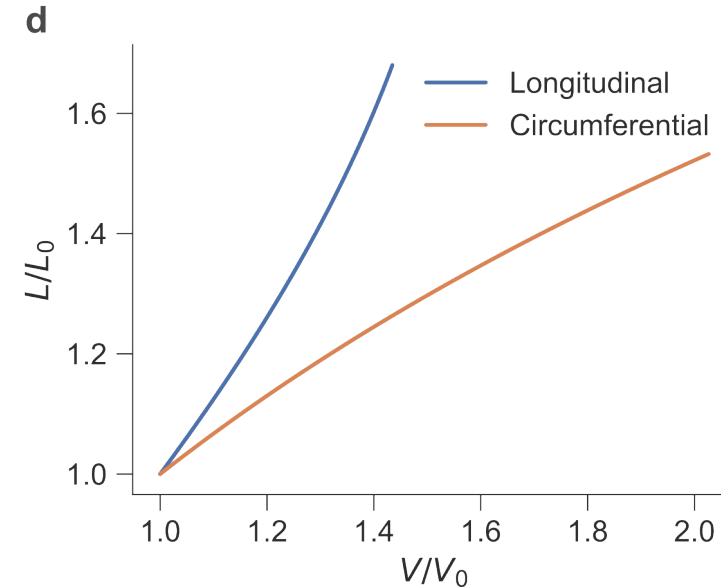
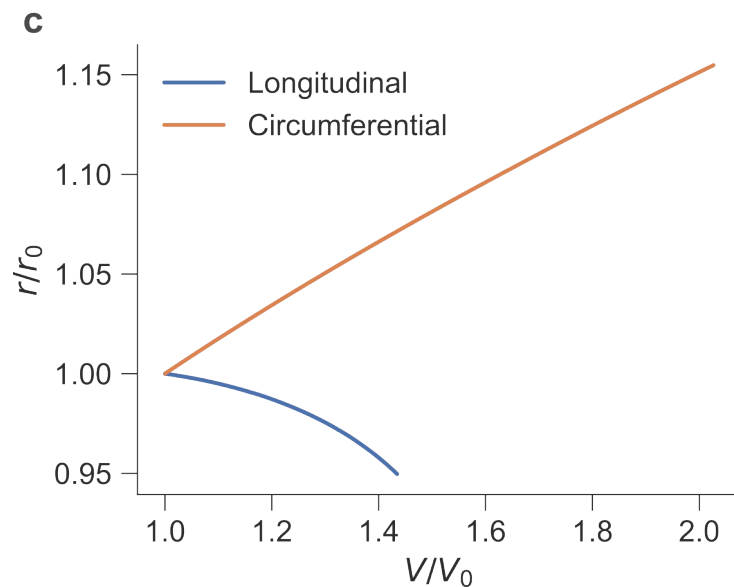
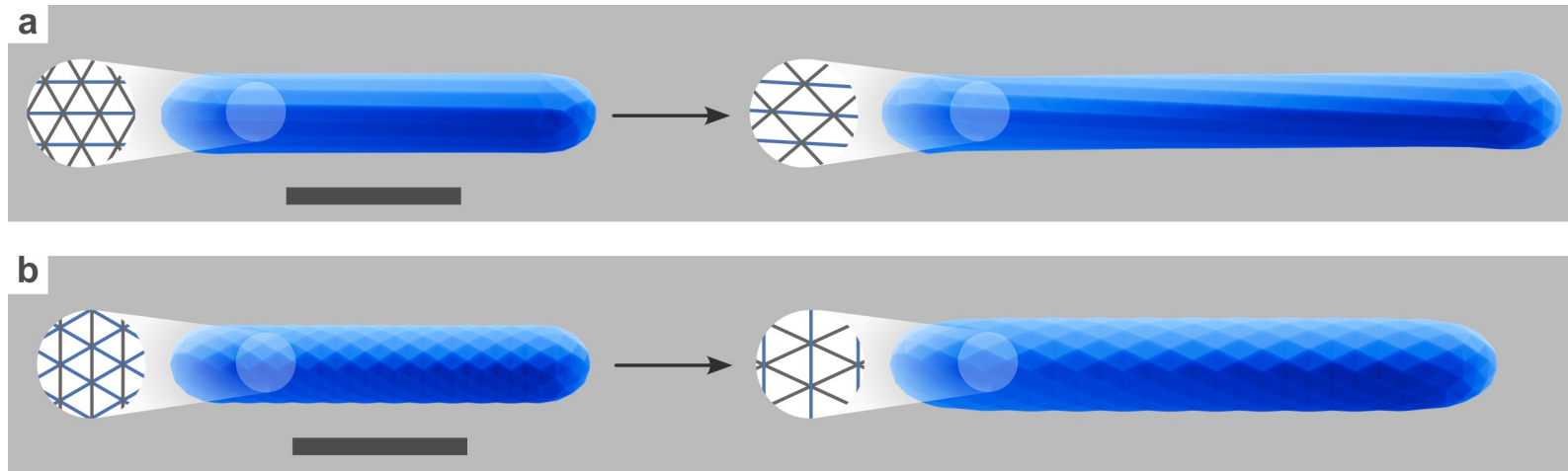
⇒ Radius is not conserved



Directed growth: Mesh alignment

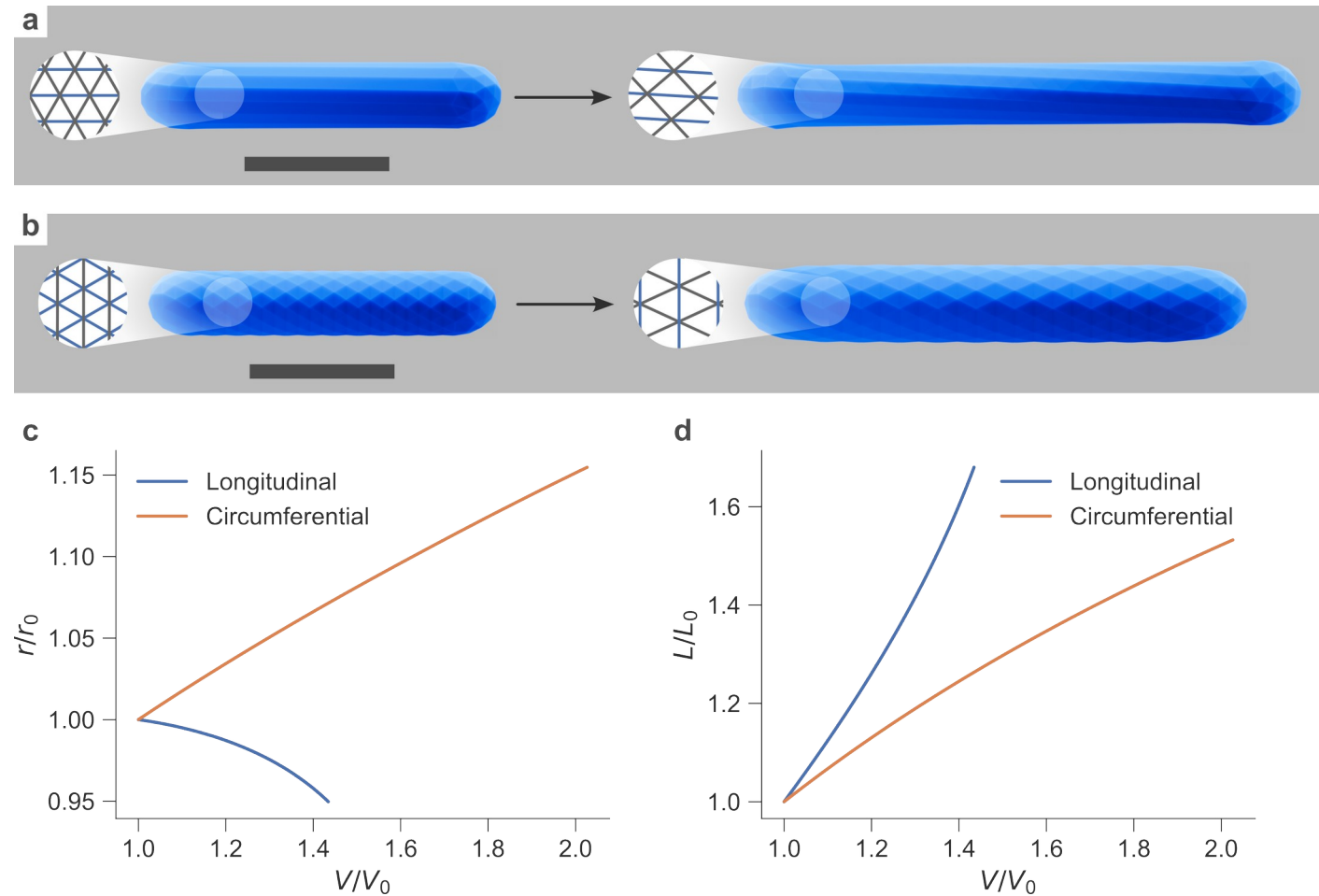


Directed growth: Mesh alignment



Spring-based model: Limitations

- Dependence on *mesh alignment*
- Acute angles in triangles → Not linear elastic
- Hyperelasticity

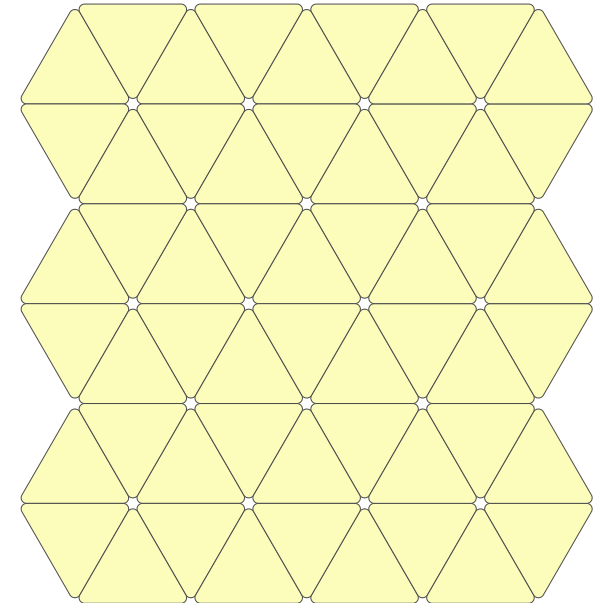


→ Alternative model

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Finite element method

- Method to solve partial differential equations (PDEs)
- Solve for deformations of complex geometries under outside forces
- Surface is divided into elements
- Solution is evaluated at nodes
- Interpolated for a full solution



Finite element method

Strain for triangular element:

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} = \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ 2\varepsilon_{12} \end{bmatrix} = \begin{bmatrix} \frac{\partial N_a}{\partial x_1} & 0 & \frac{\partial N_b}{\partial x_1} & 0 & \frac{\partial N_c}{\partial x_1} & 0 \\ 0 & \frac{\partial N_a}{\partial x_2} & 0 & \frac{\partial N_b}{\partial x_2} & 0 & \frac{\partial N_c}{\partial x_2} \\ \frac{\partial N_a}{\partial x_1} & \frac{\partial N_a}{\partial x_2} & \frac{\partial N_b}{\partial x_1} & \frac{\partial N_b}{\partial x_2} & \frac{\partial N_c}{\partial x_1} & \frac{\partial N_c}{\partial x_2} \end{bmatrix} \begin{bmatrix} u_1^{(a)} \\ u_2^{(a)} \\ u_1^{(b)} \\ u_2^{(b)} \\ u_1^{(c)} \\ u_2^{(c)} \end{bmatrix}$$

Finite element method

Strain for triangular element:

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Stress-strain relation:

$$\begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \end{bmatrix} = [D] \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{12} \end{bmatrix} = \frac{E}{(1-\nu)^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & (1-\nu)/2 \end{bmatrix} \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{12} \end{bmatrix}$$

Finite element method

Strain for triangular element:

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} = \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ 2\varepsilon_{12} \end{bmatrix} = \begin{bmatrix} \frac{\partial N_a}{\partial x_1} & 0 & \frac{\partial N_b}{\partial x_1} & 0 & \frac{\partial N_c}{\partial x_1} & 0 \\ 0 & \frac{\partial N_a}{\partial x_2} & 0 & \frac{\partial N_b}{\partial x_2} & 0 & \frac{\partial N_c}{\partial x_2} \\ \frac{\partial N_a}{\partial x_1} & \frac{\partial N_a}{\partial x_2} & \frac{\partial N_b}{\partial x_1} & \frac{\partial N_b}{\partial x_2} & \frac{\partial N_c}{\partial x_1} & \frac{\partial N_c}{\partial x_2} \end{bmatrix} \begin{bmatrix} u_1^{(a)} \\ u_2^{(a)} \\ u_1^{(b)} \\ u_2^{(b)} \\ u_1^{(c)} \\ u_2^{(c)} \end{bmatrix}$$

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Strain energy:

$$U = \frac{1}{2} \vec{\varepsilon}^T \vec{\sigma} = \frac{1}{2} \vec{\varepsilon}^T [D] \vec{\varepsilon}.$$

Finite element method

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} \quad U = \frac{1}{2}\vec{\varepsilon}^T \vec{\sigma} = \frac{1}{2}\vec{\varepsilon}^T [D]\vec{\varepsilon}.$$

Finite element method

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} \quad U = \frac{1}{2}\vec{\varepsilon}^{\mathbf{T}}\vec{\sigma} = \frac{1}{2}\vec{\varepsilon}^{\mathbf{T}}[D]\vec{\varepsilon}.$$

Strain energy for element:

$$W_{\text{element}} = \frac{1}{2}\vec{u}_{\text{element}}^{\mathbf{T}}(A_{\text{element}}[B]^{\mathbf{T}}[D][B])\vec{u}_{\text{element}}$$

Finite element method

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} \quad U = \frac{1}{2}\vec{\varepsilon}^{\mathbf{T}}\vec{\sigma} = \frac{1}{2}\vec{\varepsilon}^{\mathbf{T}}[D]\vec{\varepsilon}.$$

Strain energy for element:

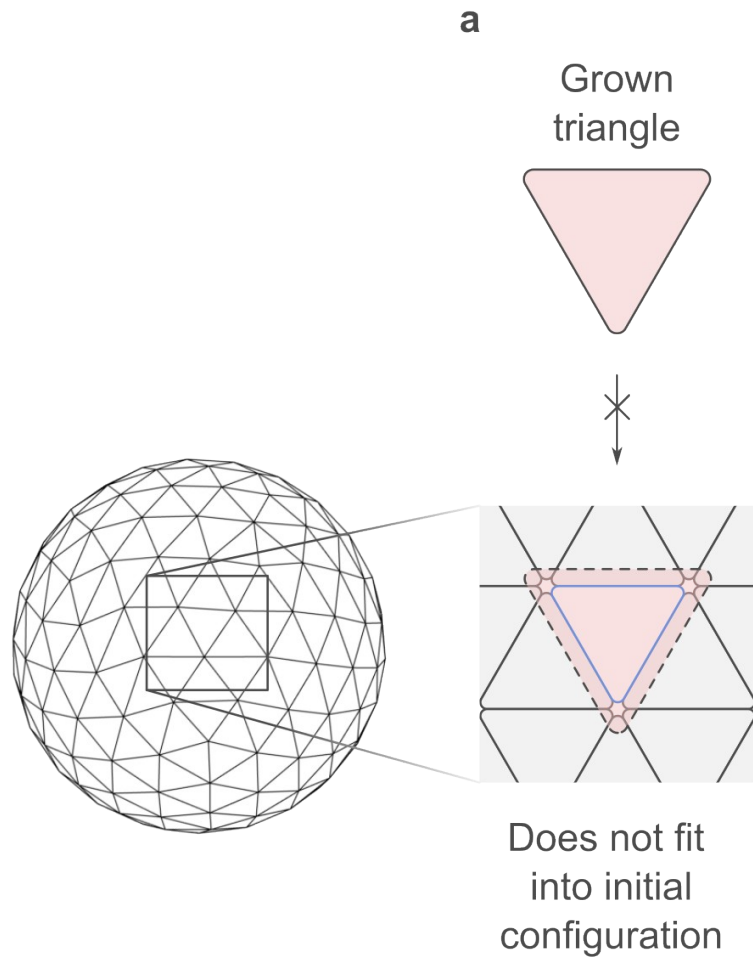
$$W_{\text{element}} = \frac{1}{2}\vec{u}_{\text{element}}^{\mathbf{T}}(A_{\text{element}}[B]^{\mathbf{T}}[D][B])\vec{u}_{\text{element}}$$

Total strain energy:

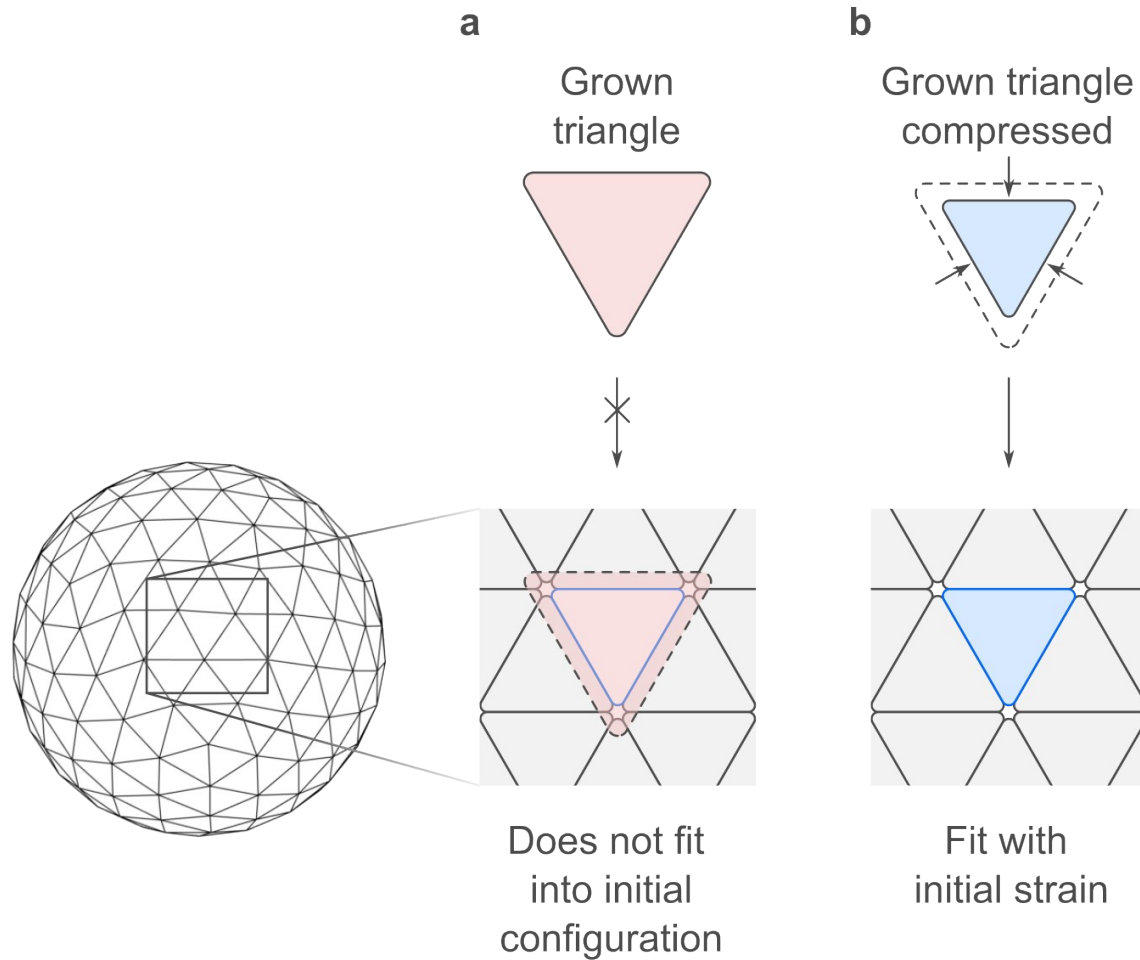
$$W = \sum_{\text{elements}} W_{\text{element}} = \frac{1}{2} \sum_{\text{elements}} \vec{u}_{\text{element}}^{\mathbf{T}} K_{\text{element}} \vec{u}_{\text{element}}$$

Minimize W with respect to $u \rightarrow$ Deformations

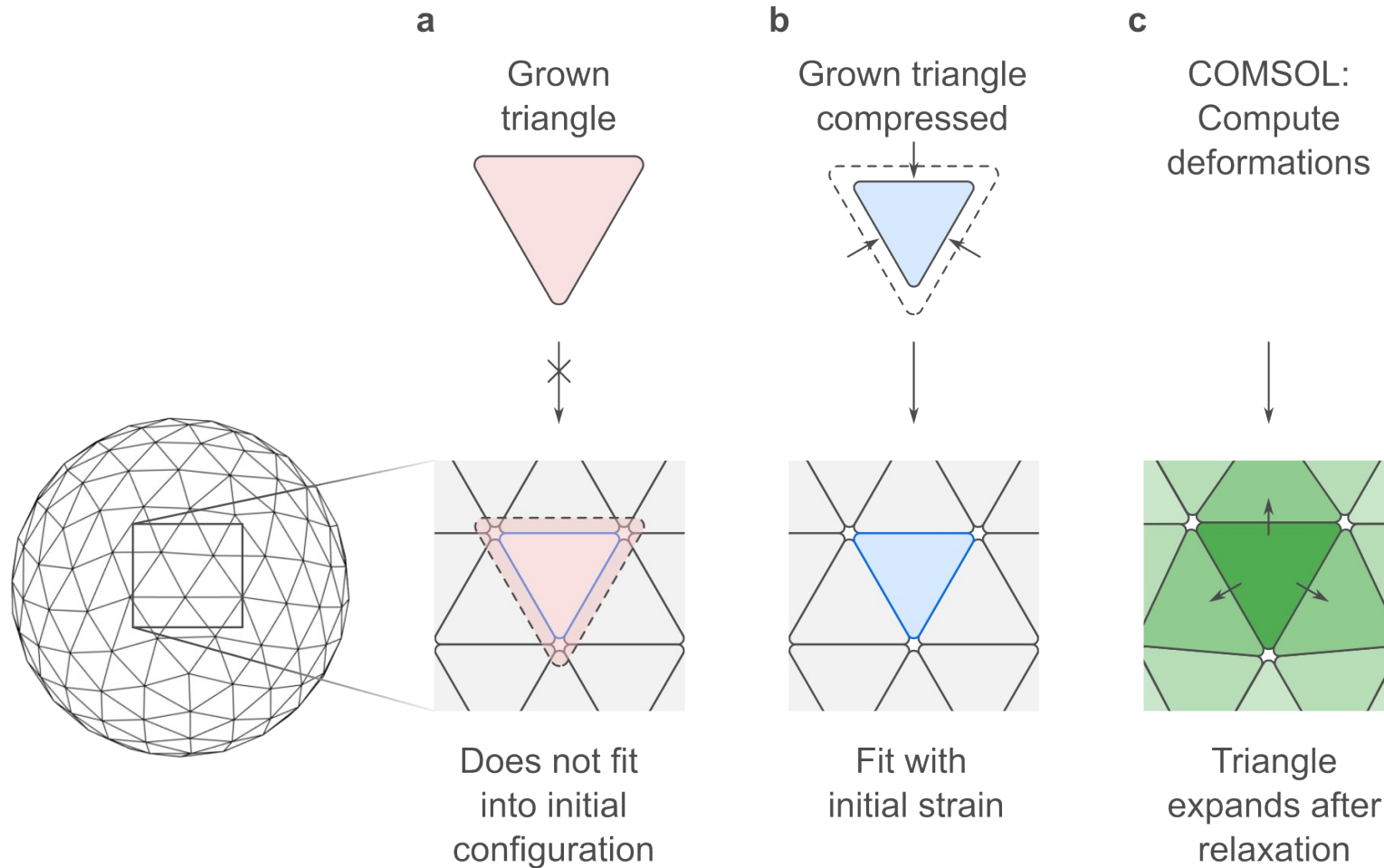
Finite-element-based Model



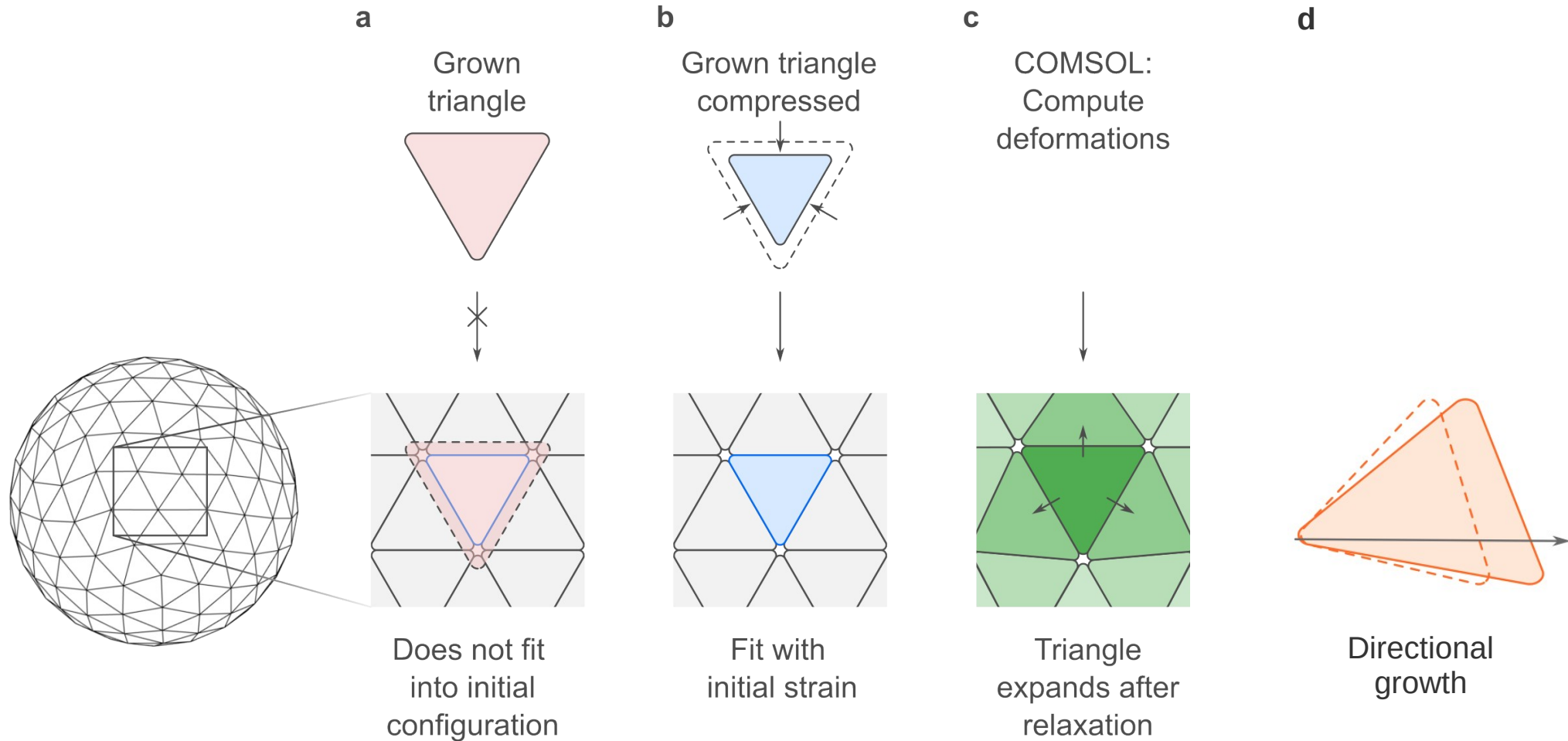
Finite-element-based Model



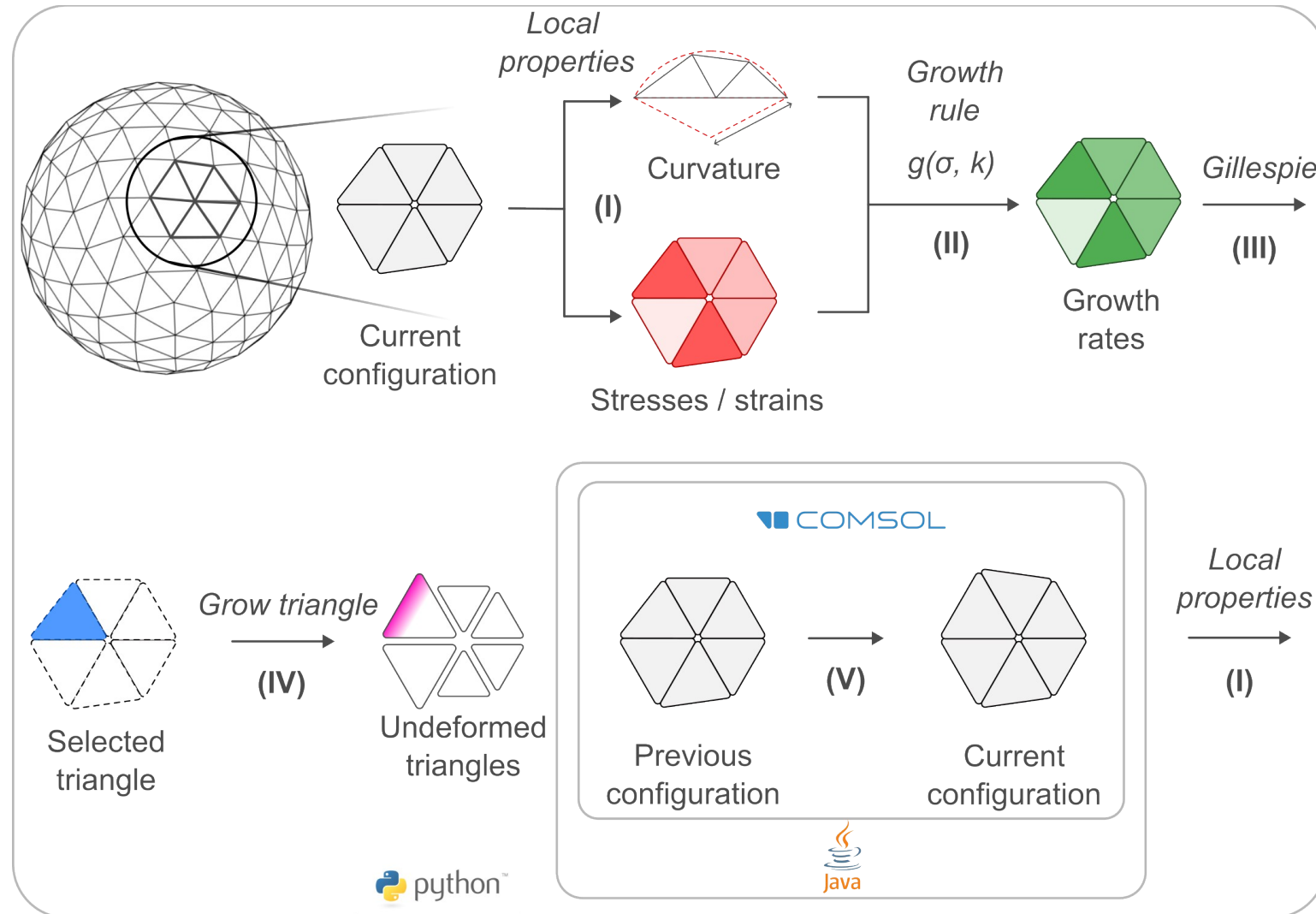
Finite-element-based Model



Finite-element-based Model

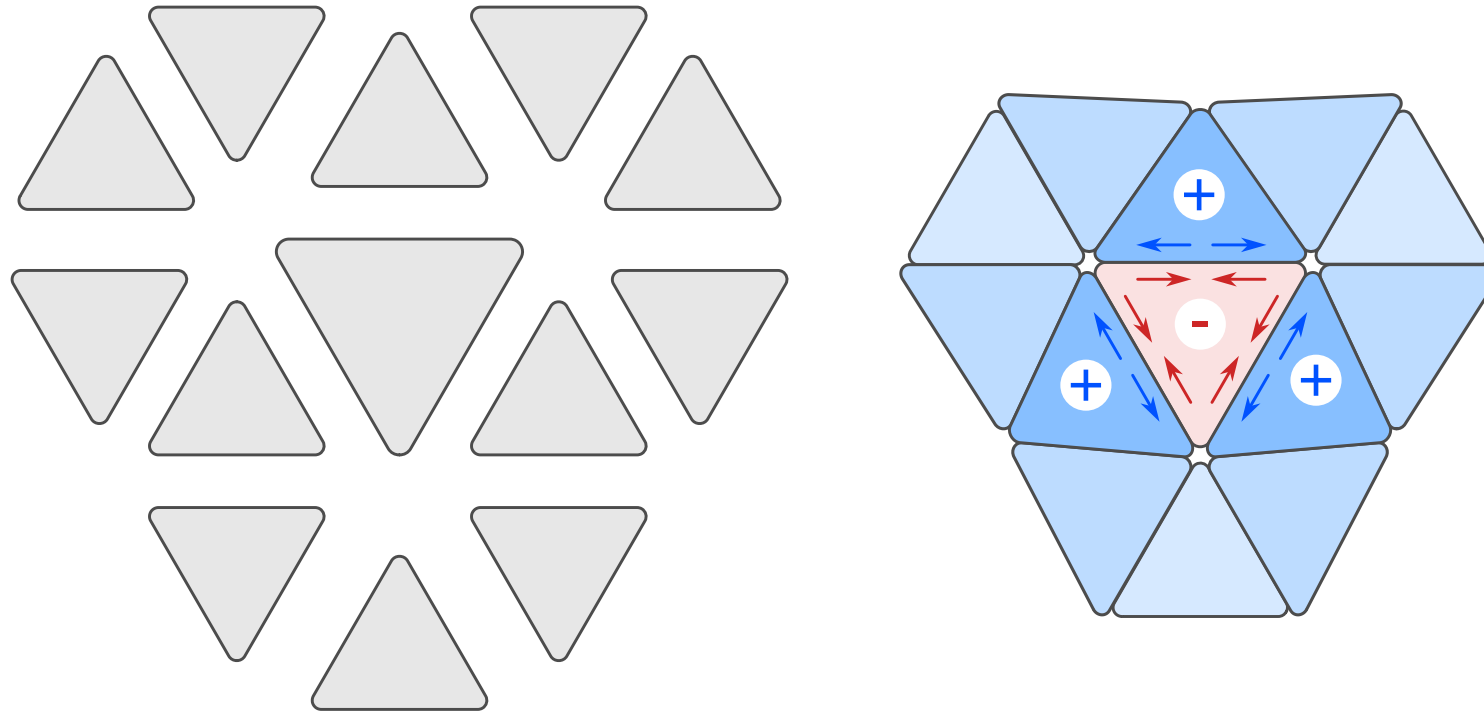


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Observable: Surface stresses



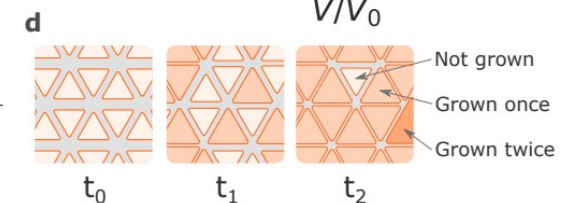
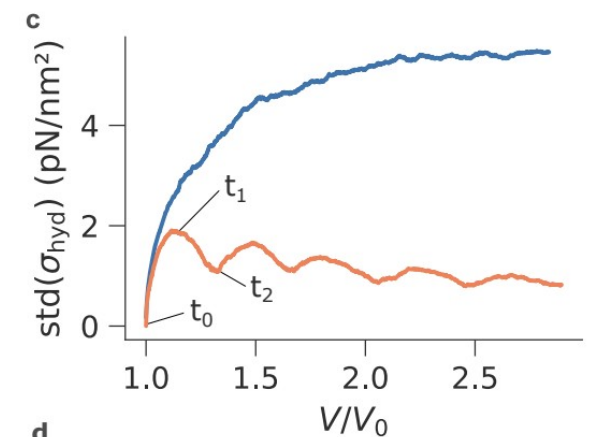
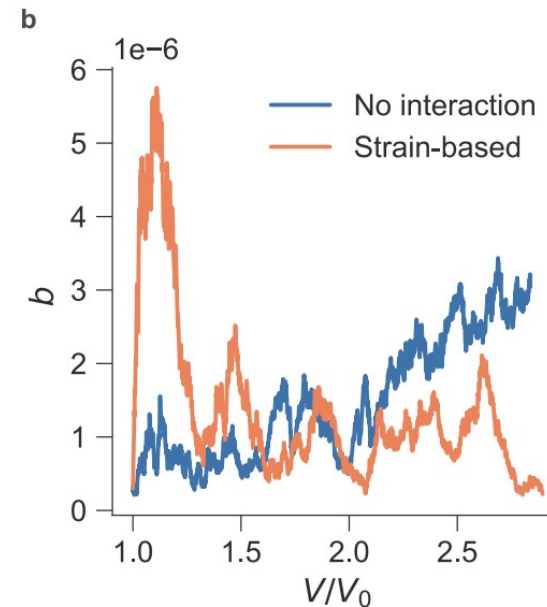
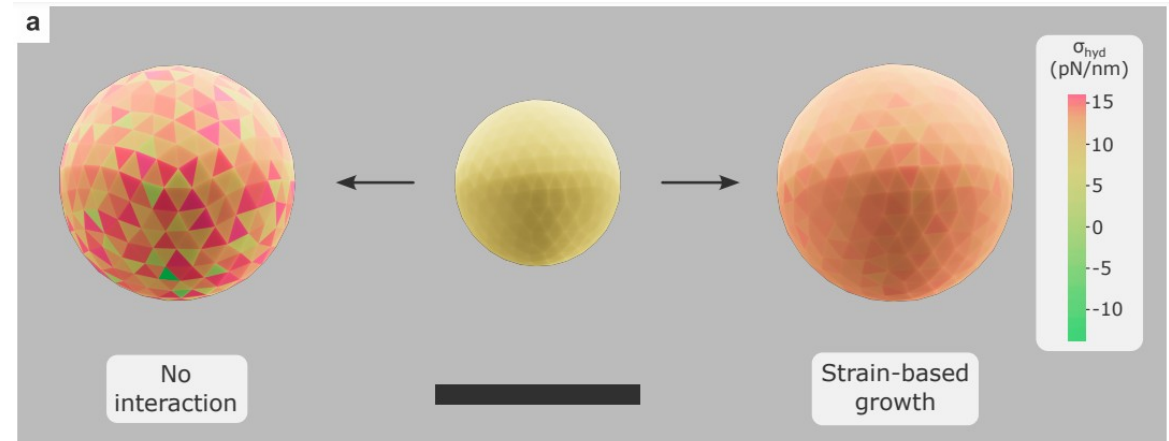
Size mismatch of elements

- High **compressive** and **tensile** stresses
- Affects mechanical stability

Random vs. strain-based growth

Strain-based growth rates:

$$\lambda^{(e)} = -\lambda_0 + \lambda_1 \varepsilon_h^{(e)}$$



Random vs. strain-based growth

Strain-based growth rates:

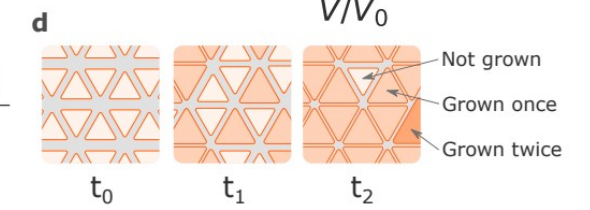
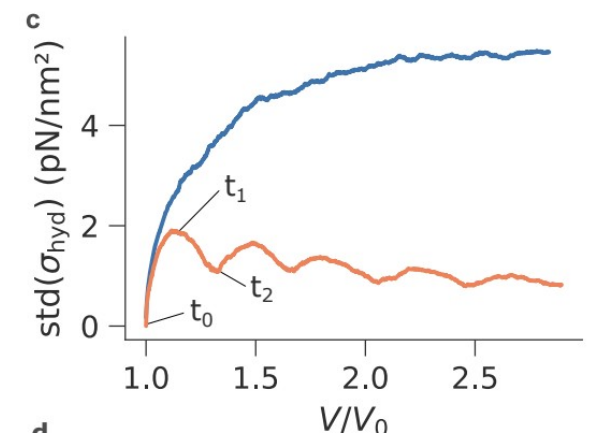
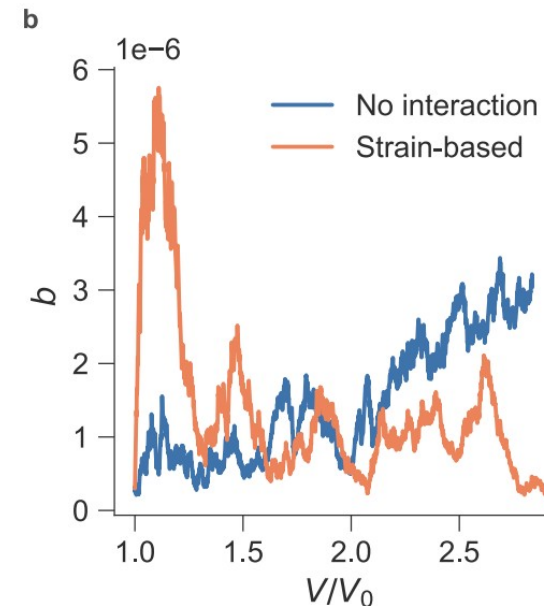
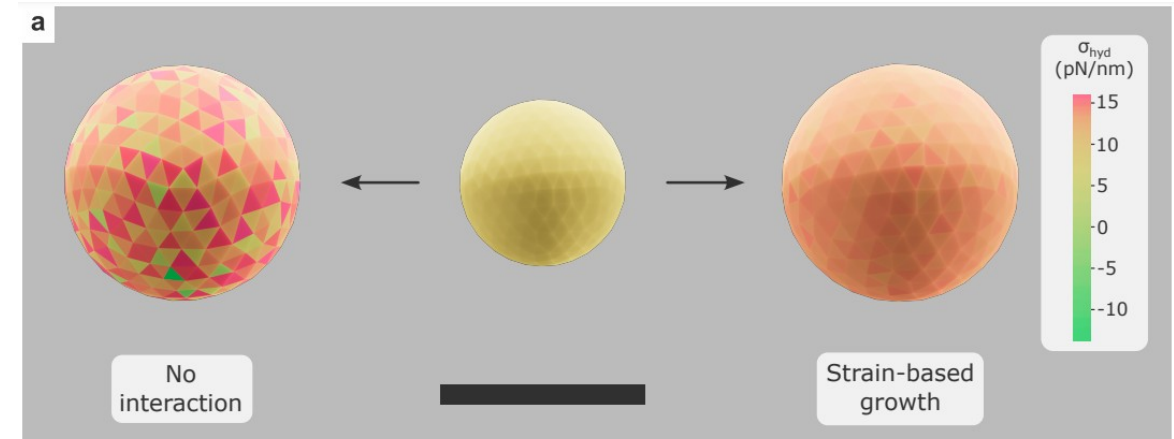
$$\lambda^{(e)} = -\lambda_0 + \lambda_1 \varepsilon_h^{(e)}$$

Random

- Spherical shape
- **High** surface stresses

Strain-based

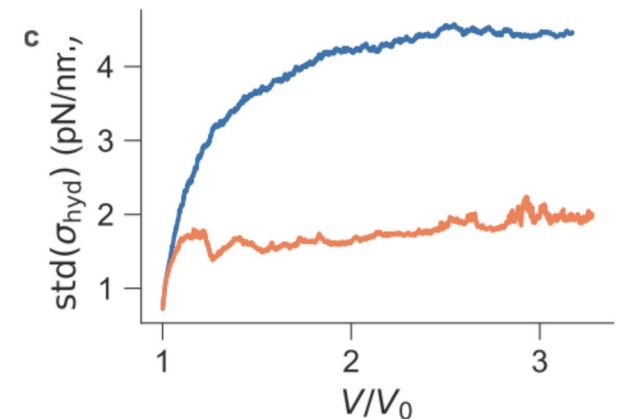
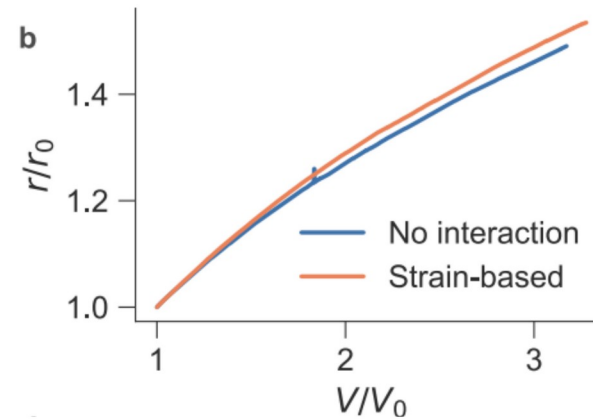
- Spherical shape
- **Moderate** surface stresses



Random vs. strain-based growth

Strain-based growth rates:

$$\lambda^{(e)} = -\lambda_0 + \lambda_1 \varepsilon_h^{(e)}$$



Random vs. strain-based growth

Strain-based growth rates:

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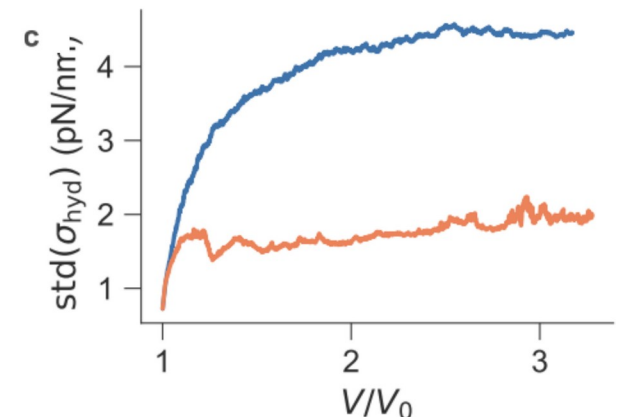
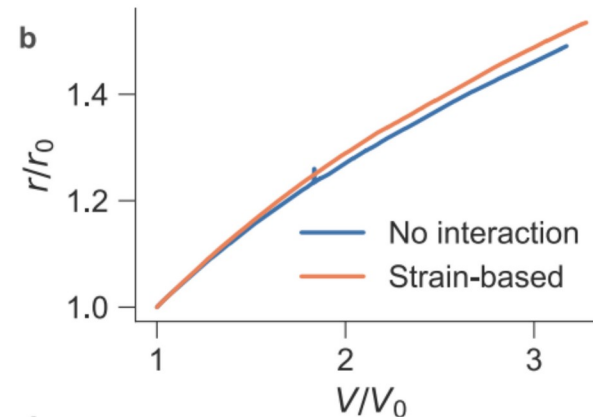
Random

- Spherical shape
- **High** stresses

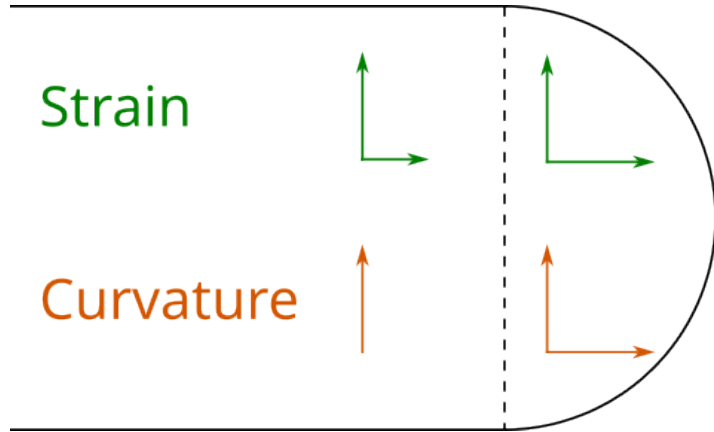
Strain-based

- Spherical shape
- **Moderate** stresses

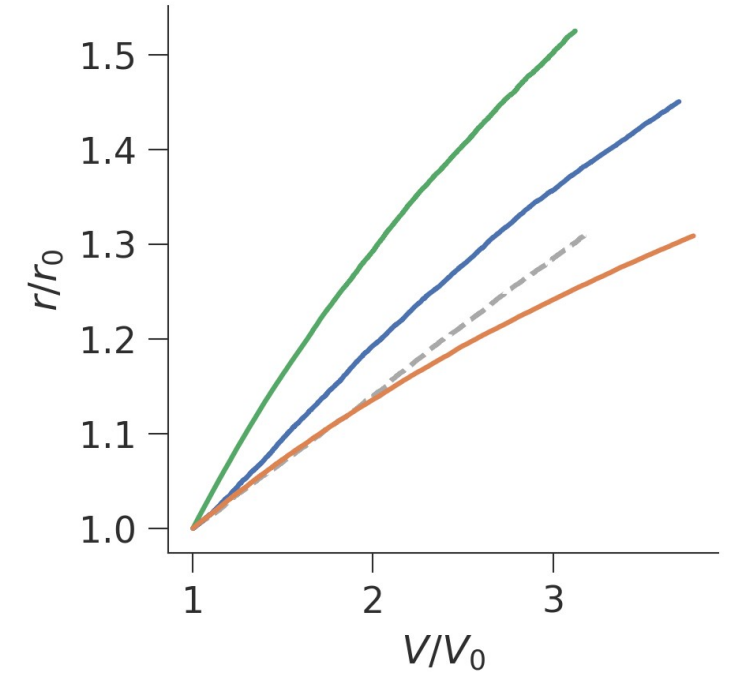
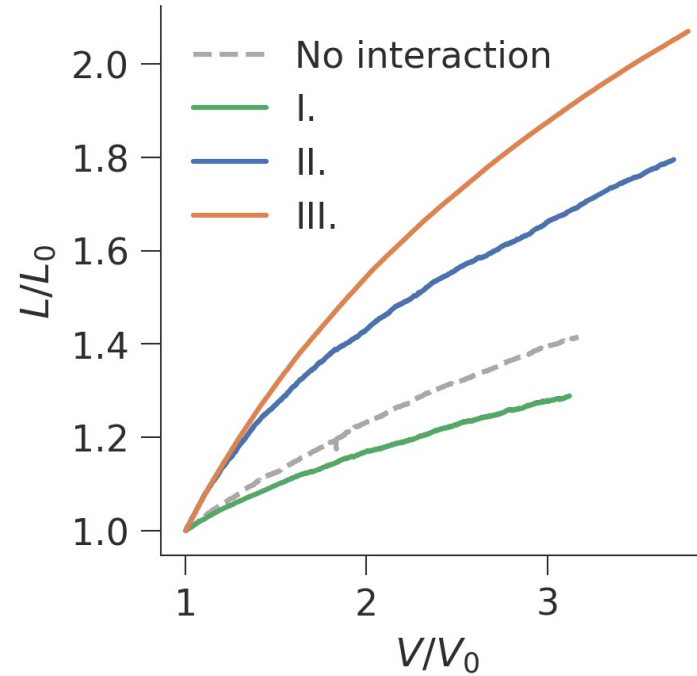
⇒ Radius is not conserved



Directional Growth: Strain / Curvature



| | Location | Direction |
|------|-----------|-----------|
| I. | Strain | Strain |
| II. | Curvature | Strain |
| III. | Curvature | Curvature |

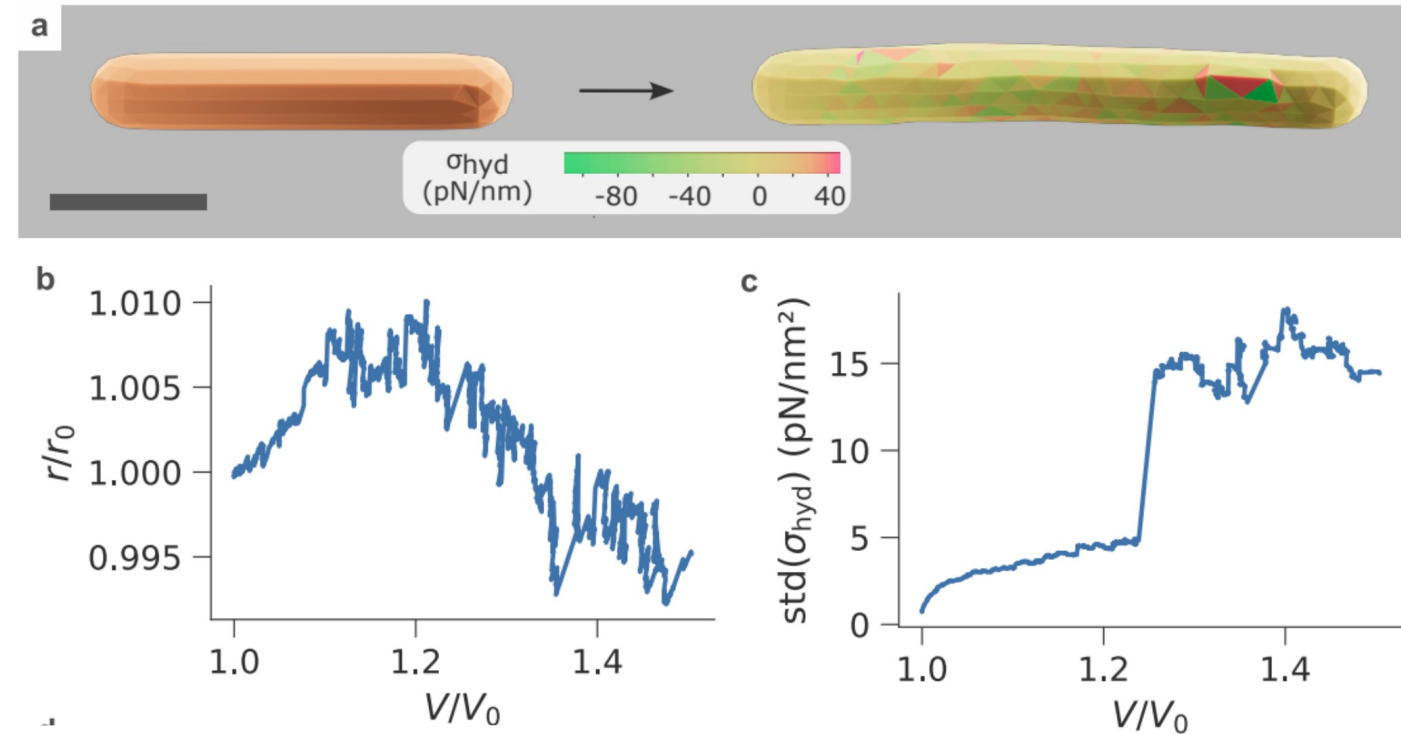


Correction mechanism

Combination

longitudinal: +
 circumferential: -

- Elongation
- Radius is conserved
- Problem: Large stresses



- Introduction
- Spring-based model
 - Idea behind the model
 - Results
- Finite-element-based model
 - Idea behind the model
 - Results
- **Summary**
- Outlook

Summary

- Implemented two physical models of the bacterial shell
- Limitations of the spring-based model
- Solved with finite-element-based model
- Strain-based growth improved the mechanical stability
- Importance of a correction mechanism

- Introduction
- Spring-based model
 - Idea behind the model
 - Results
- Finite-element-based model
 - Idea behind the model
 - Results
- Summary
- **Outlook**

Outlook

- Understanding high stresses
- Explore the parameter space
 - Gram-positive bacteria: Higher pressures, thicker cell wall
 - Pressure changes during growth
- Explore other geometries

Thank you

Appendix

$$Y = \frac{2}{\sqrt{3}} k_s,$$

$$\kappa_b = \frac{\sqrt{3}}{2} k_b,$$

$$\kappa_b = \frac{Et^3}{12(1-\nu)}$$

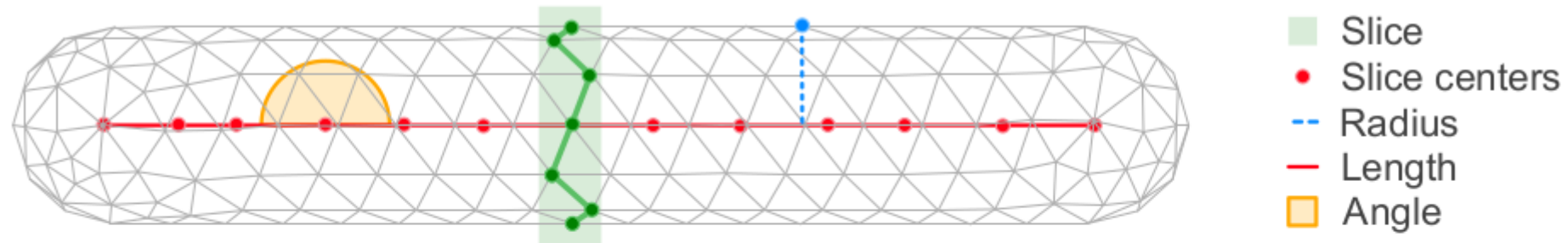
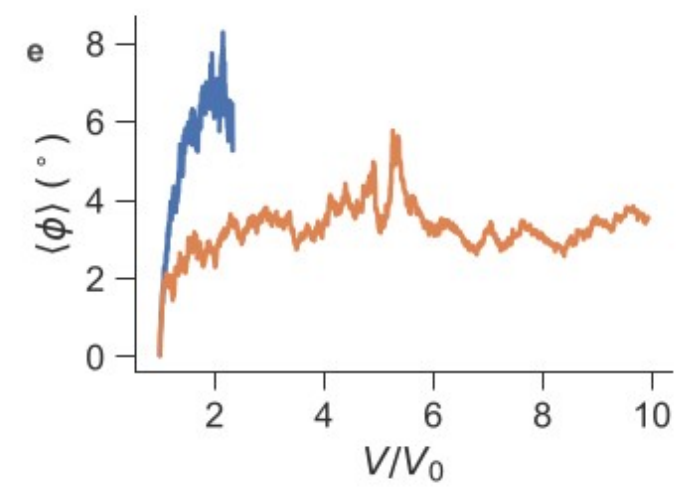
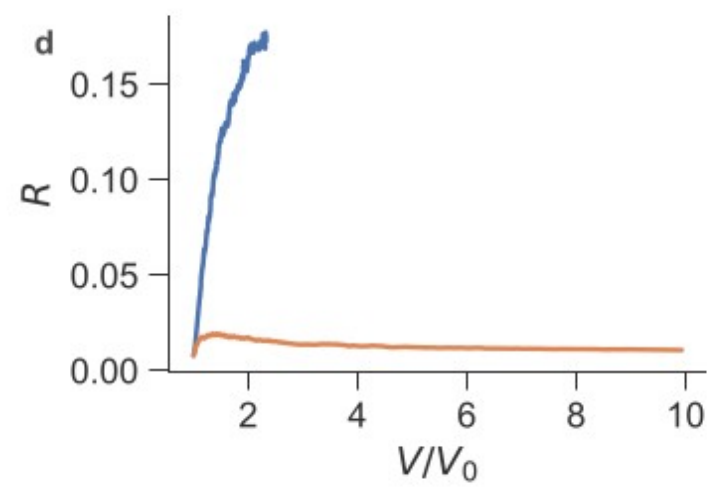
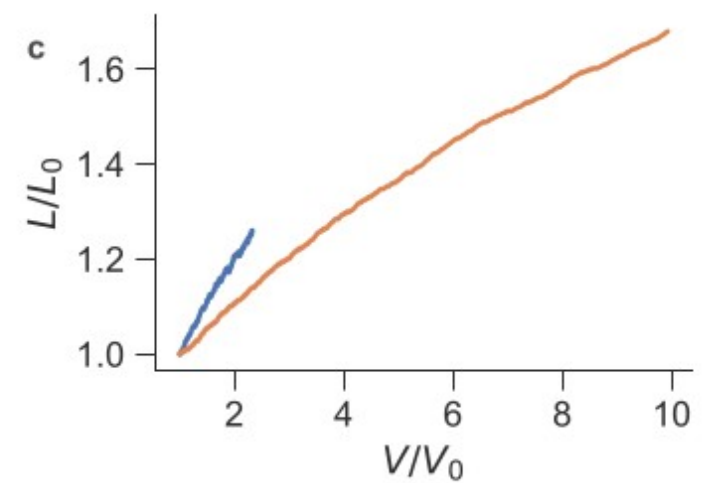
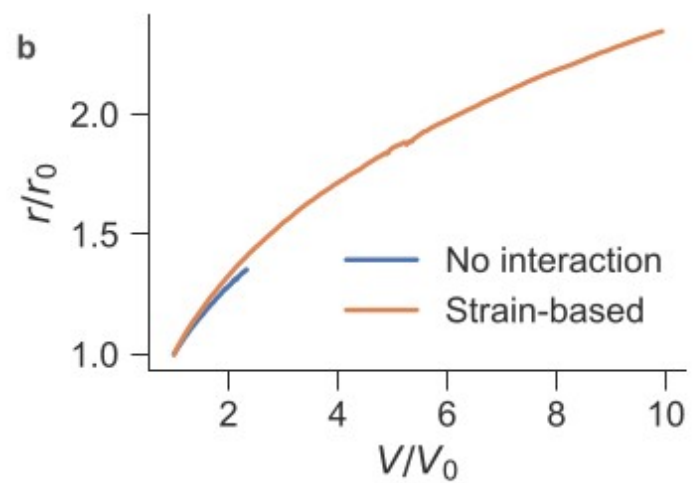
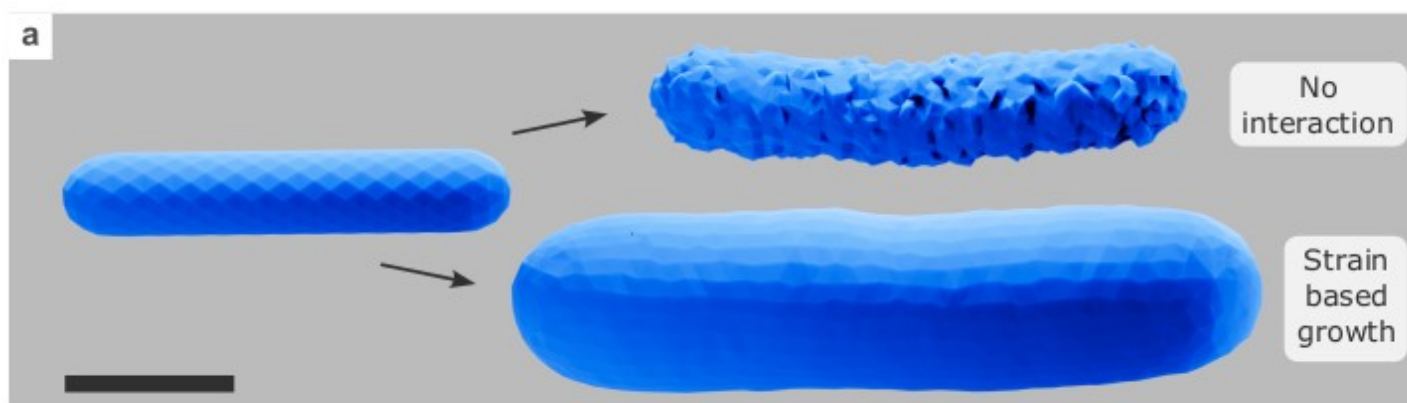
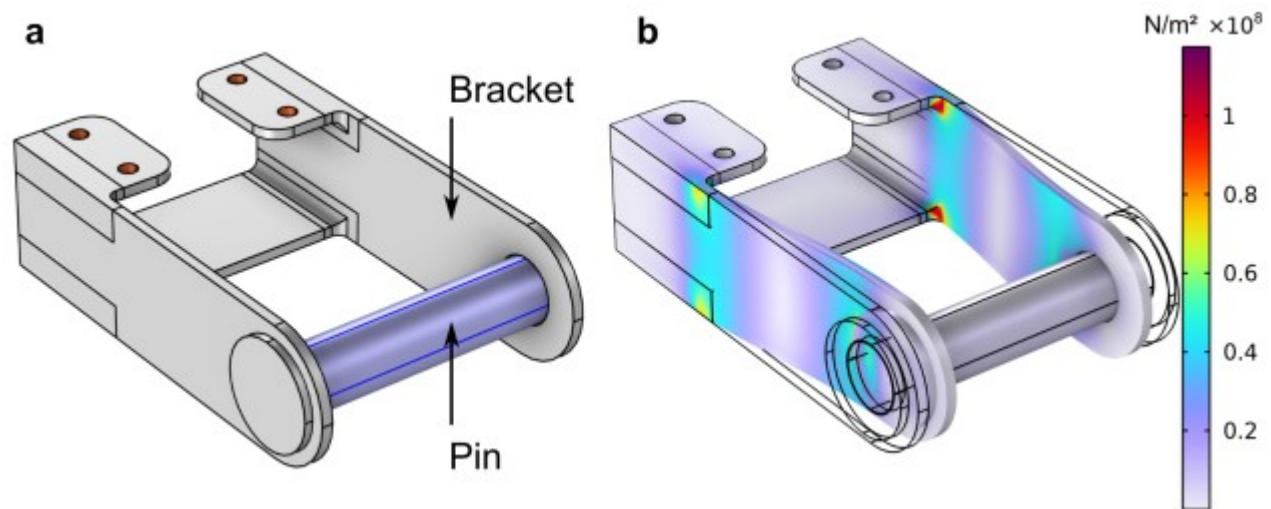
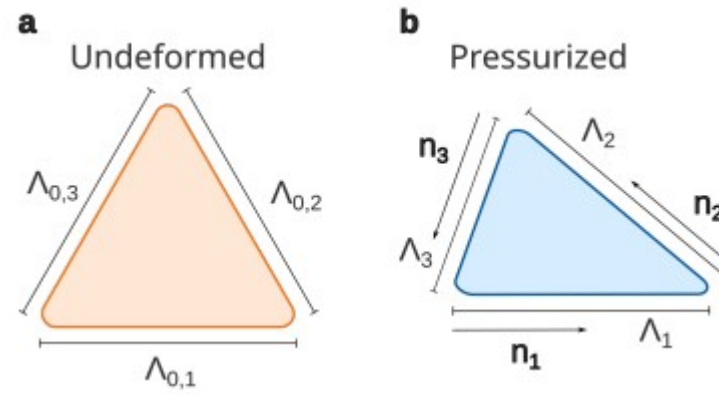


Figure 2.3.4: Computing length, radius and bending angle of the rod-shaped shell.

The shell is divided into slices (green) along its length. At initialization, each vertex is assigned a slice. The gravitational centers of the slices (red dots) can be computed at any point in the simulation. Radius, length and bending angles are computed from the line connecting the slice centers.



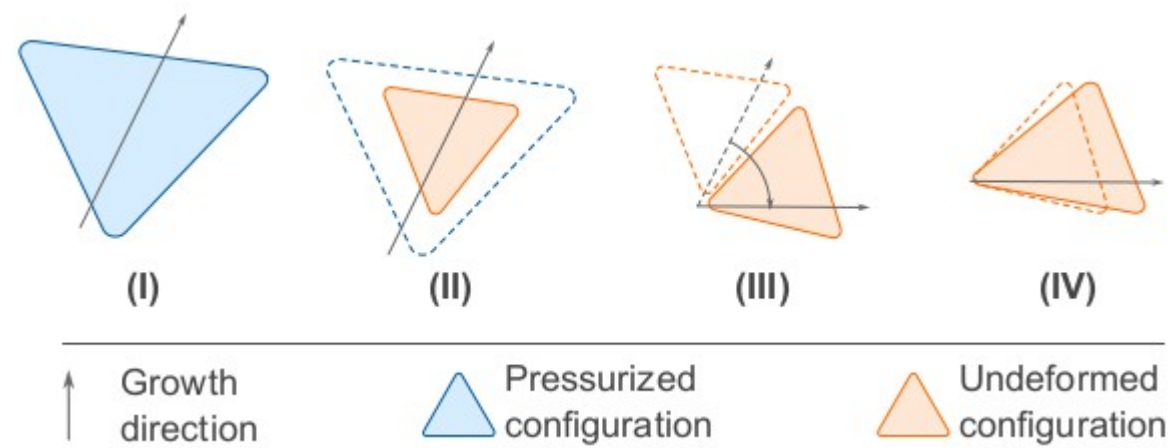


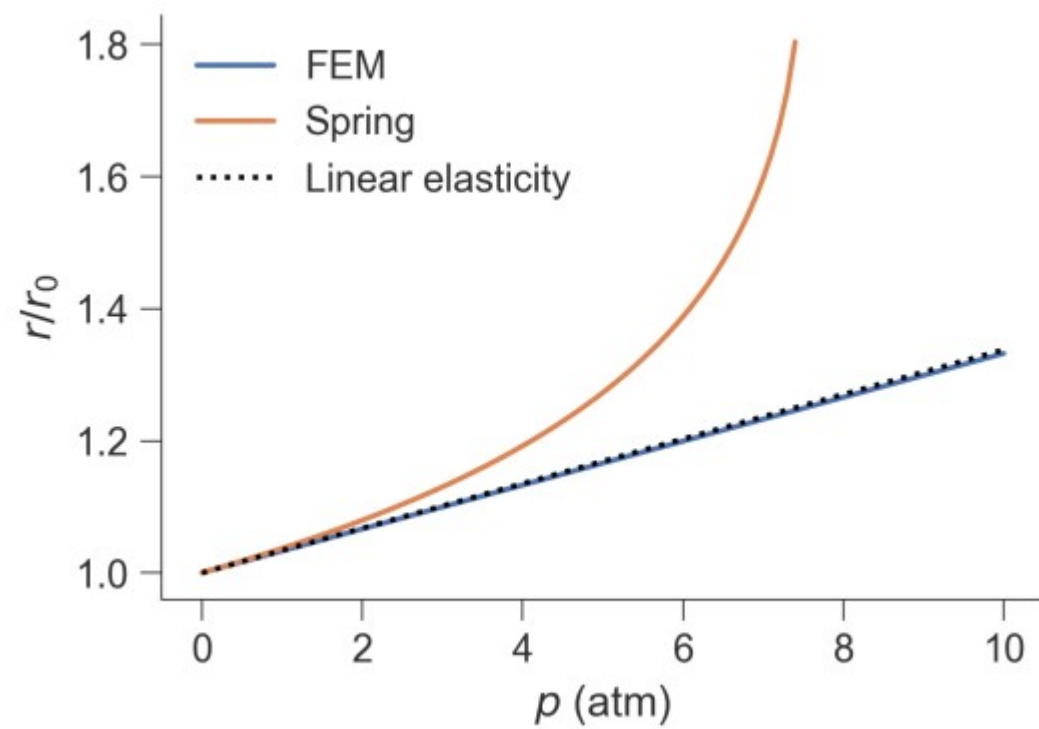


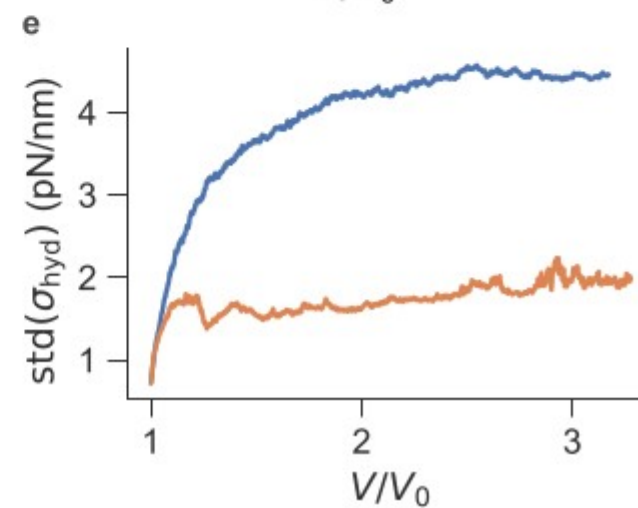
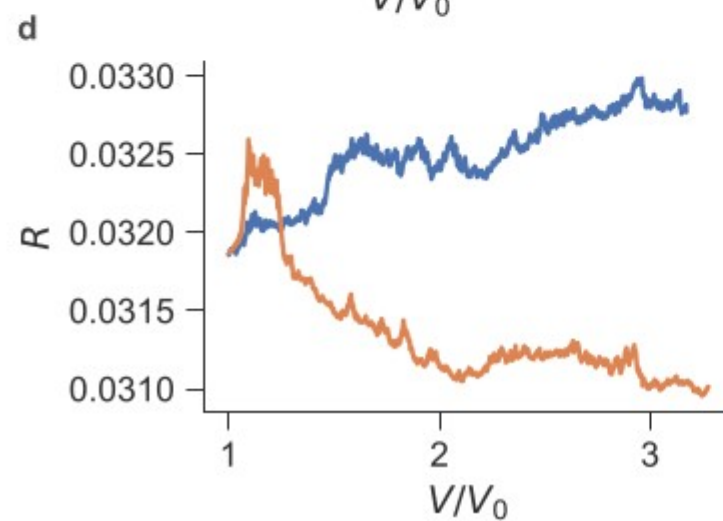
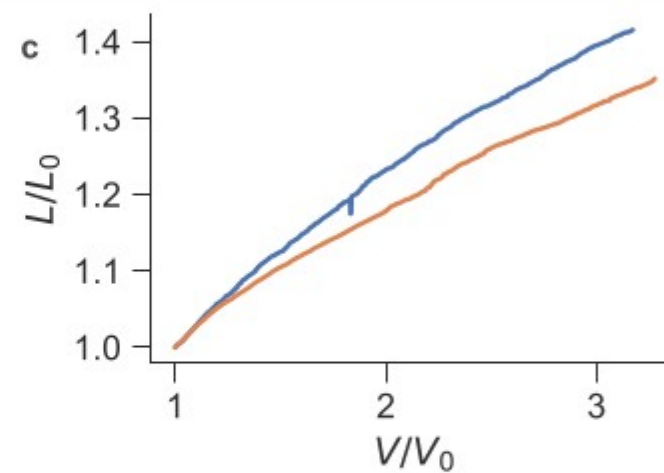
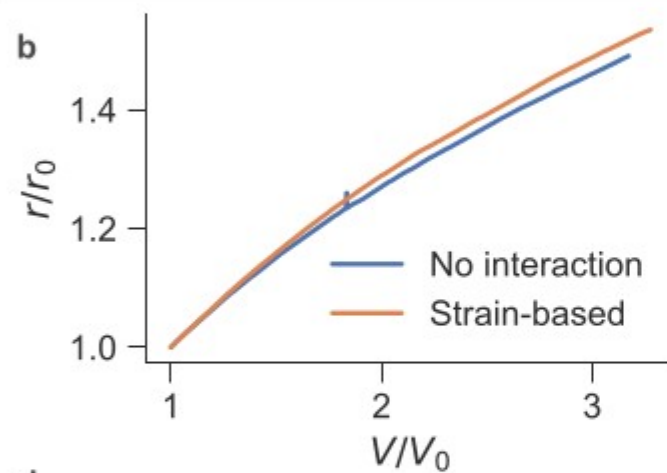
$$\varepsilon(\vec{n}^{(i)}) = \frac{\Lambda_i - \Lambda_{i,0}}{\Lambda_i}$$

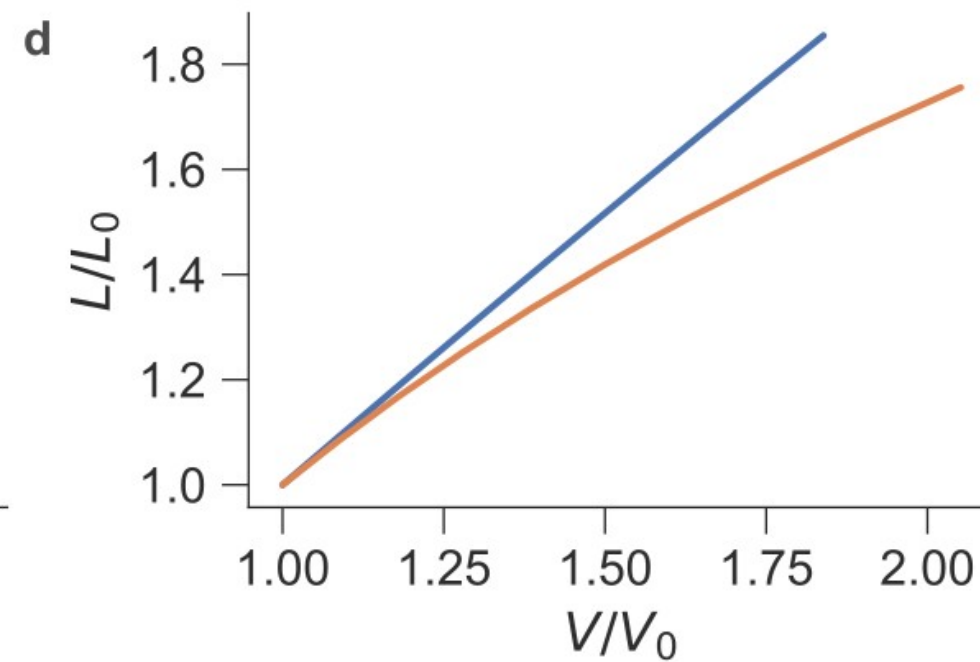
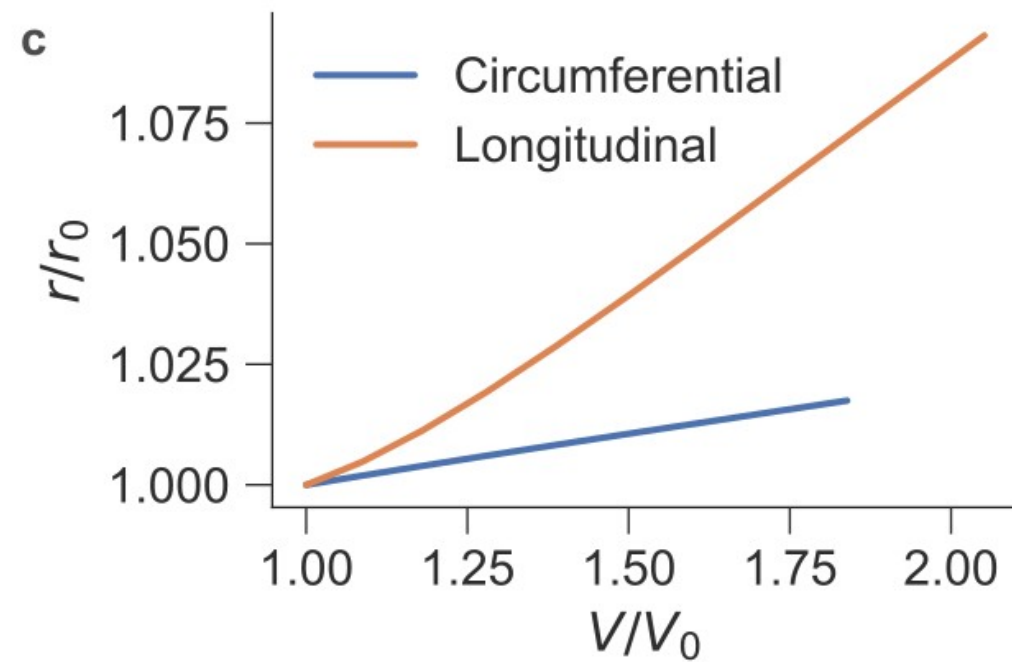
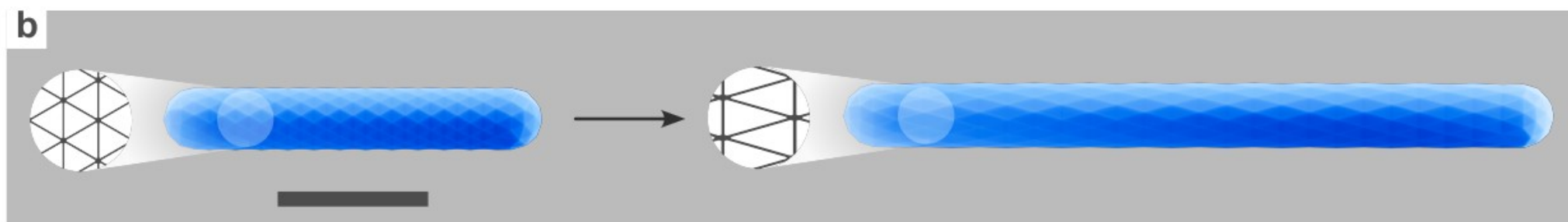
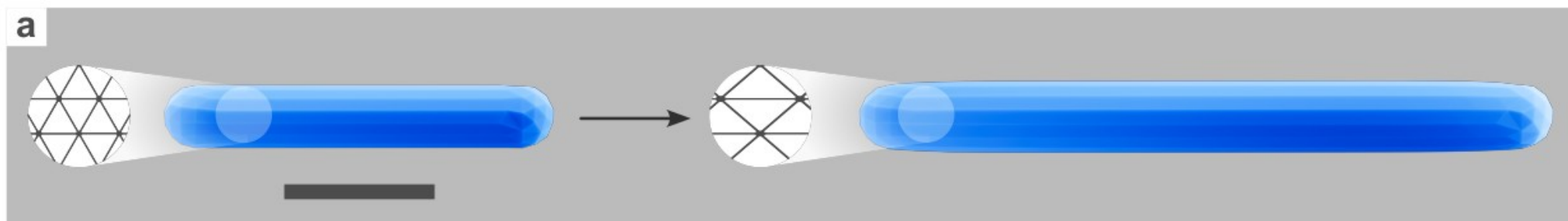
$$\varepsilon_{\text{direction}}(\vec{n}^{(i)}) = \varepsilon_{kl} n_k^{(i)} n_l^{(i)},$$

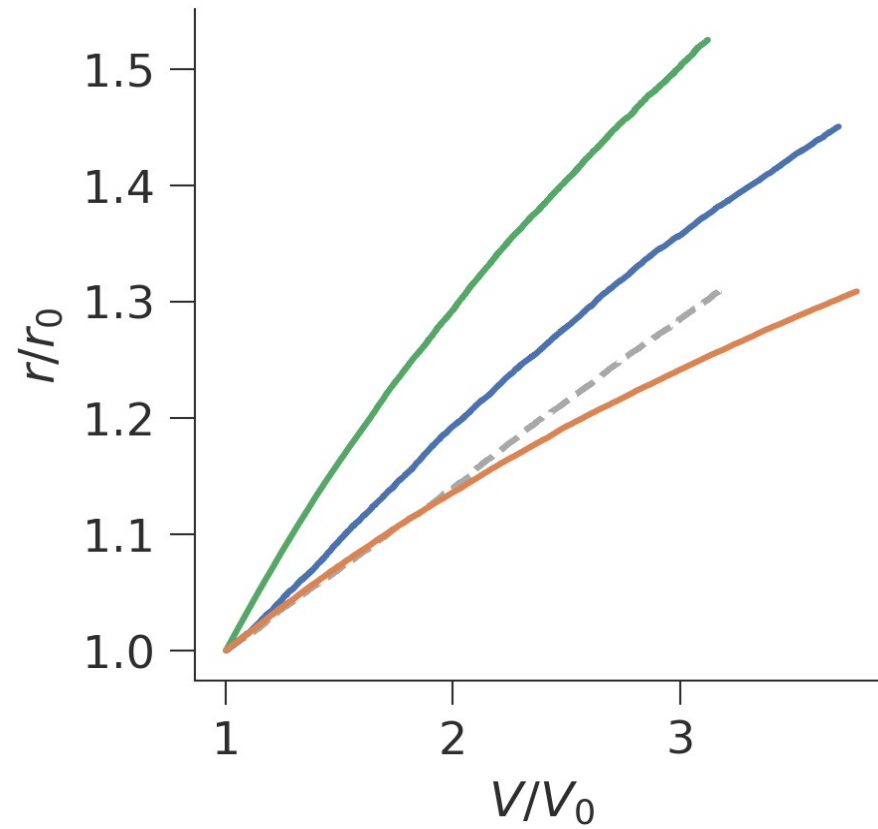
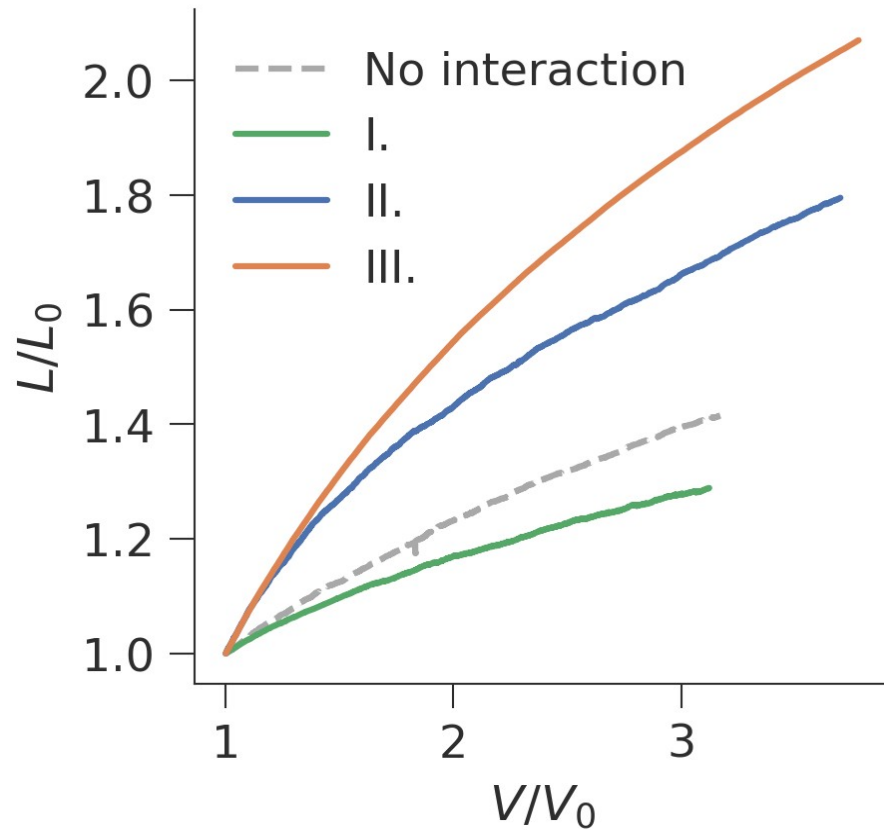
$$\begin{bmatrix} \varepsilon_{\text{direction}}(\vec{n}^{(1)}) \\ \varepsilon_{\text{direction}}(\vec{n}^{(2)}) \\ \varepsilon_{\text{direction}}(\vec{n}^{(3)}) \end{bmatrix} = \begin{bmatrix} n_1^{(1)} n_1^{(1)} & n_1^{(1)} n_2^{(1)} & n_2^{(1)} n_2^{(1)} \\ n_1^{(2)} n_1^{(2)} & n_1^{(2)} n_2^{(2)} & n_2^{(2)} n_2^{(2)} \\ n_1^{(3)} n_1^{(3)} & n_1^{(3)} n_2^{(3)} & n_2^{(3)} n_2^{(3)} \end{bmatrix} \cdot \begin{bmatrix} \varepsilon_{11} \\ 2\varepsilon_{12} \\ \varepsilon_{22} \end{bmatrix}$$



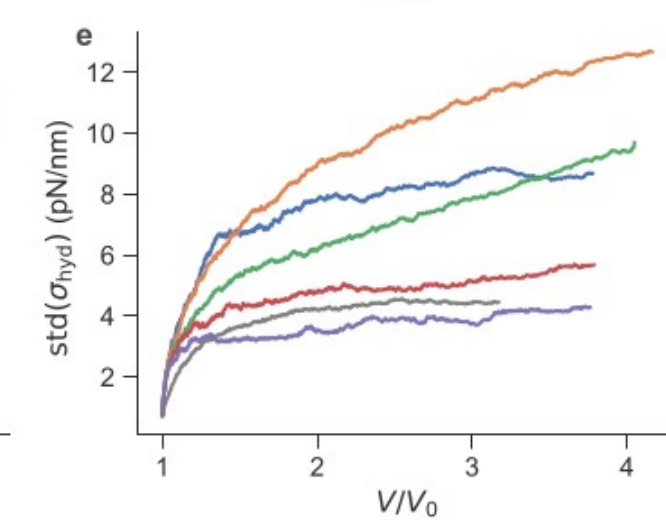
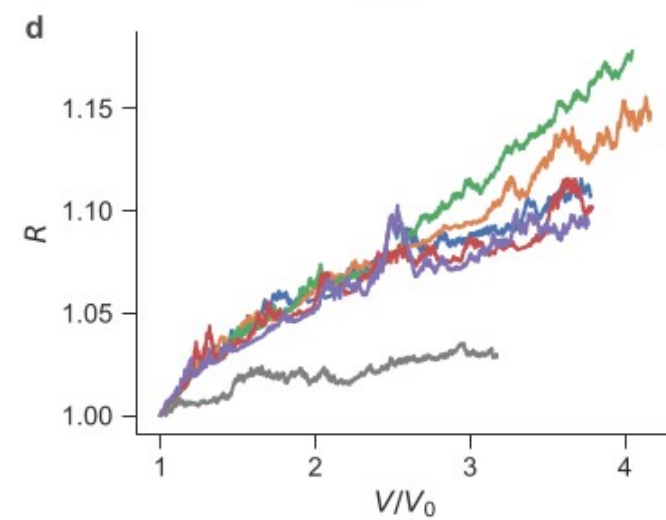
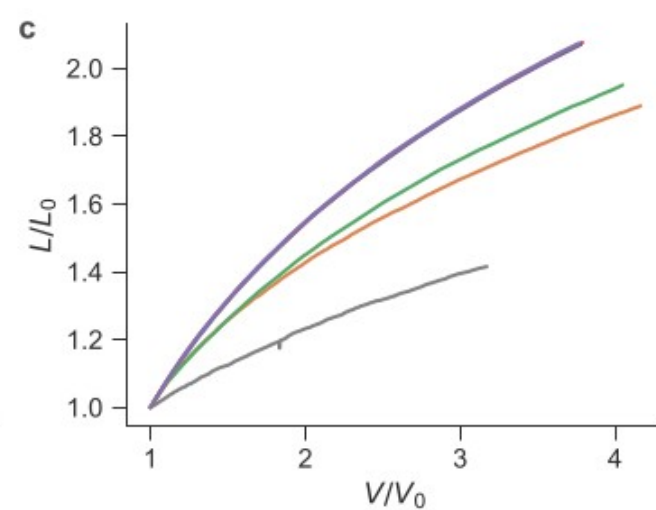
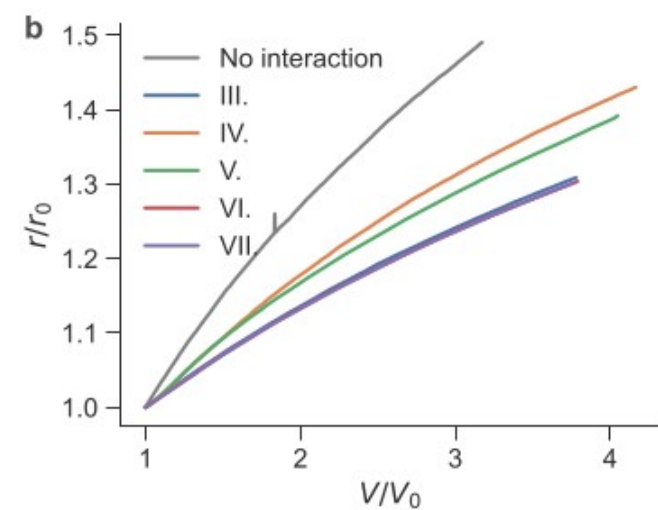
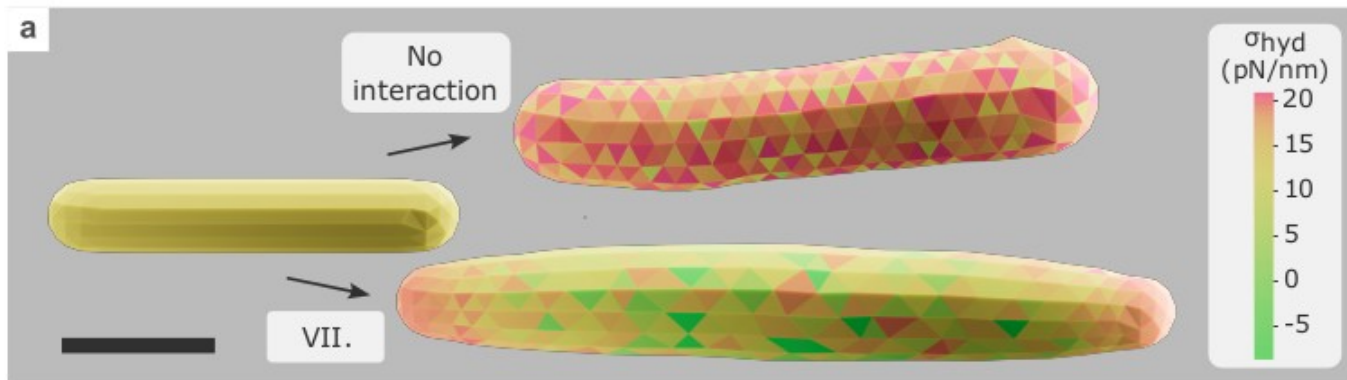








| | Growth reaction rates | Growth direction |
|------|---|----------------------|
| I. | $\lambda_0 + \lambda_1 \varepsilon_{\min} - \lambda_2 \varepsilon_{\max}$ | ε_{\min} |
| II. | $\lambda_0 + \lambda_1 K_{\min}$ | ε_{\min} |
| III. | $\lambda_0 + \lambda_1 K_{\min}$ | K_{\min} |



| | Growth reaction rates | Growth direction |
|------|--|----------------------|
| IV. | $-\lambda_0 + \lambda_1 K_{\min} + \lambda_2 \varepsilon_{\text{hyd}}$ | ε_{\min} |
| V. | $-\lambda_0 + \lambda_1 K_{\min} + \lambda_2 \varepsilon_{\min}$ | ε_{\min} |
| VI. | $-\lambda_0 + \lambda_1 K_{\min} + \lambda_2 \varepsilon_{\text{hyd}}$ | K_{\min} |
| VII. | $-\lambda_0 + \lambda_1 K_{\min} + \lambda_2 \varepsilon_{\min}$ | K_{\min} |

